



Thermal analysis in the research on materials for energy conversion

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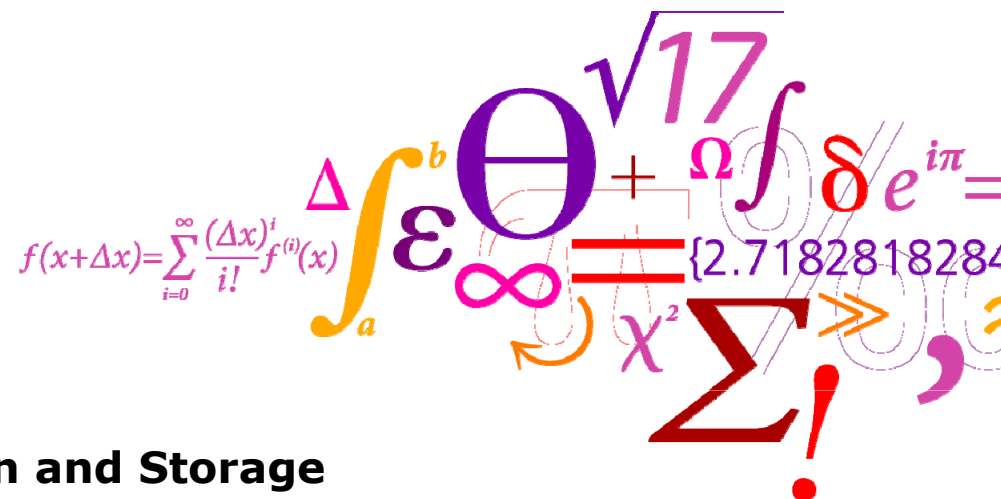
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Thermal analysis in the research on materials for energy conversion

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Risø DTU
Department of Energy Conversion and Storage

Risø Campus Technical University of Denmark



- Inaugurated 1958 as a National Laboratory
- Since 2008, part of the Technical University of Denmark
- Research on energy related technologies, e.g.
 - Wind turbines
 - Fuel cells
 - Biofuels
 - Solar cells
 - Hydrogen storage
 - Batteries
 - Energy systems
- ~600 employees



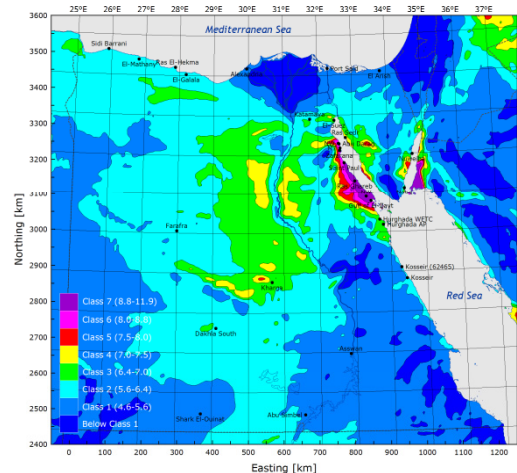
Department of Energy conversion and storage

Risø Campus Technical University of Denmark



- Inaugurated 1958 as a M
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 - Wind turbines
 - Fuel cells
 - Biofuels
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 - Hydrogen storage
 - Batteries
 - Energy systems
- ~600 employees

- **Test facility for large wind turbines**
- **Composite materials**
- **Wind atlas**



Department of Energy conversion and storage

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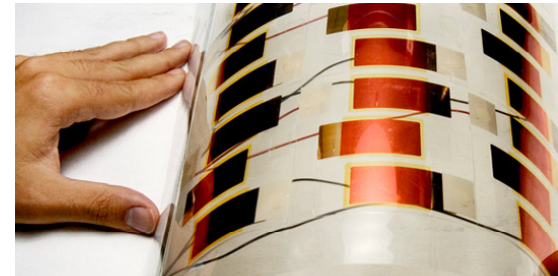


- Inaugurated 1958 as a M
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- ~600 employees

- **Polymer solar cells**

- **Produced by screen printing**

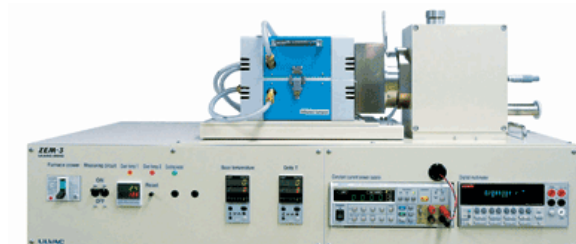
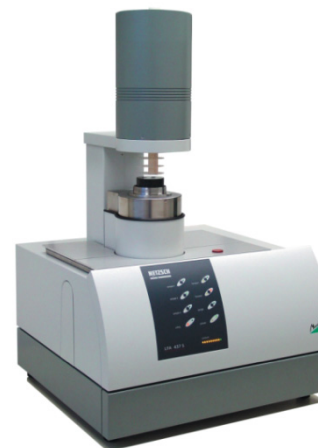
- **Flexible and cheap**



Department of Energy conversion and storage

Technologies

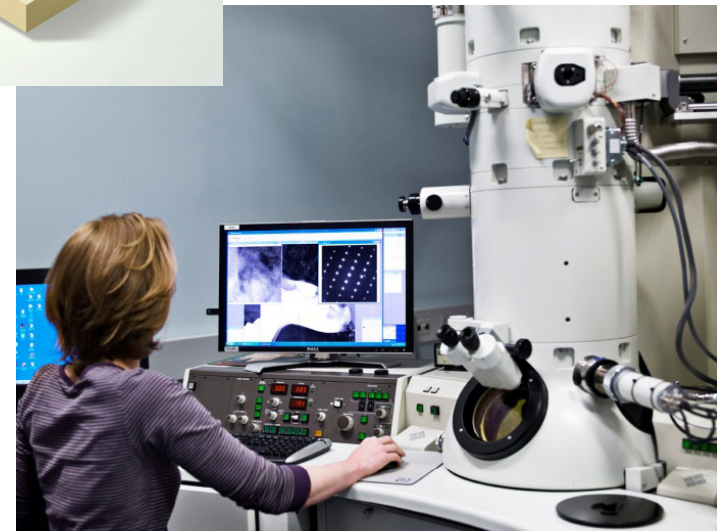
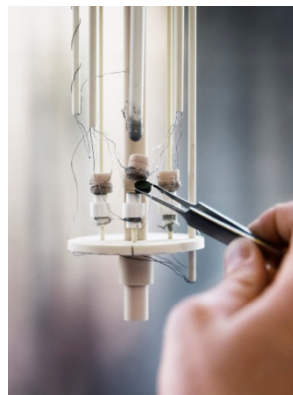
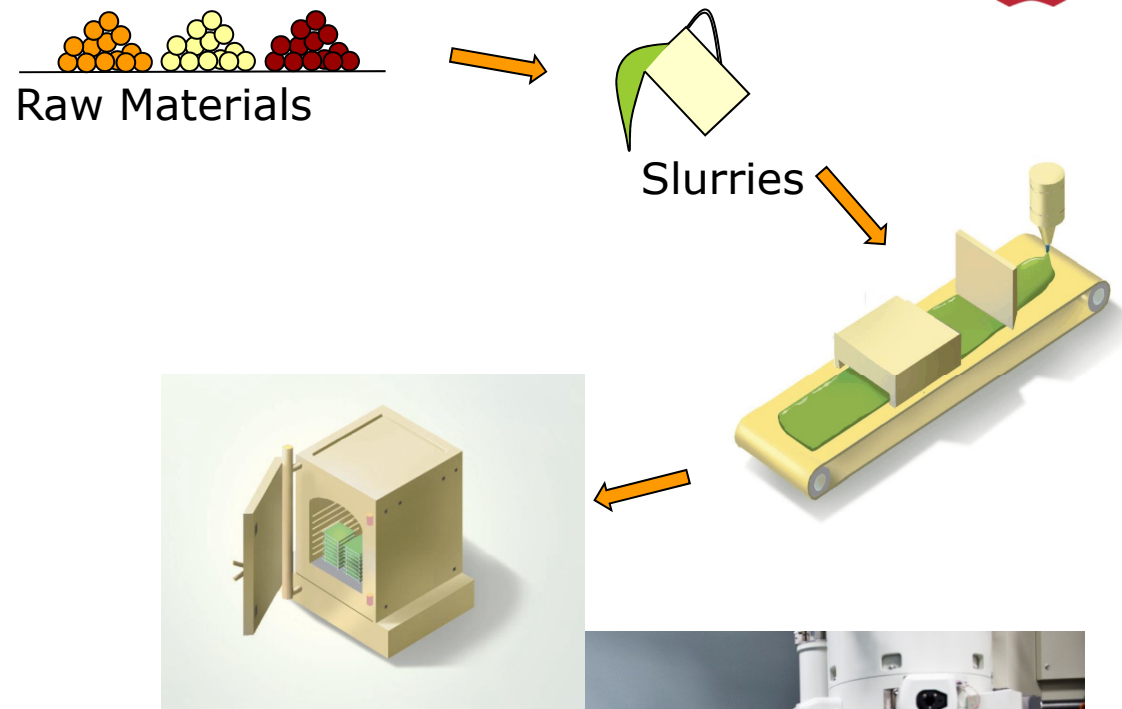
- Solid Oxide Fuel Cells
- High temperature electrolysis
- High temperature PEM fuel cells
- Polymer Photo Voltaics
- Magnetic refrigeration
- Membranes for oxygen or hydrogen separation
- Flue gas purification
- Thermoelectrics
- Batteries
- Hydrogen storage



Research on solid oxide materials



- Ceramic processing
- Materials development
- Characterization
- Testing in-situ
- Modelling



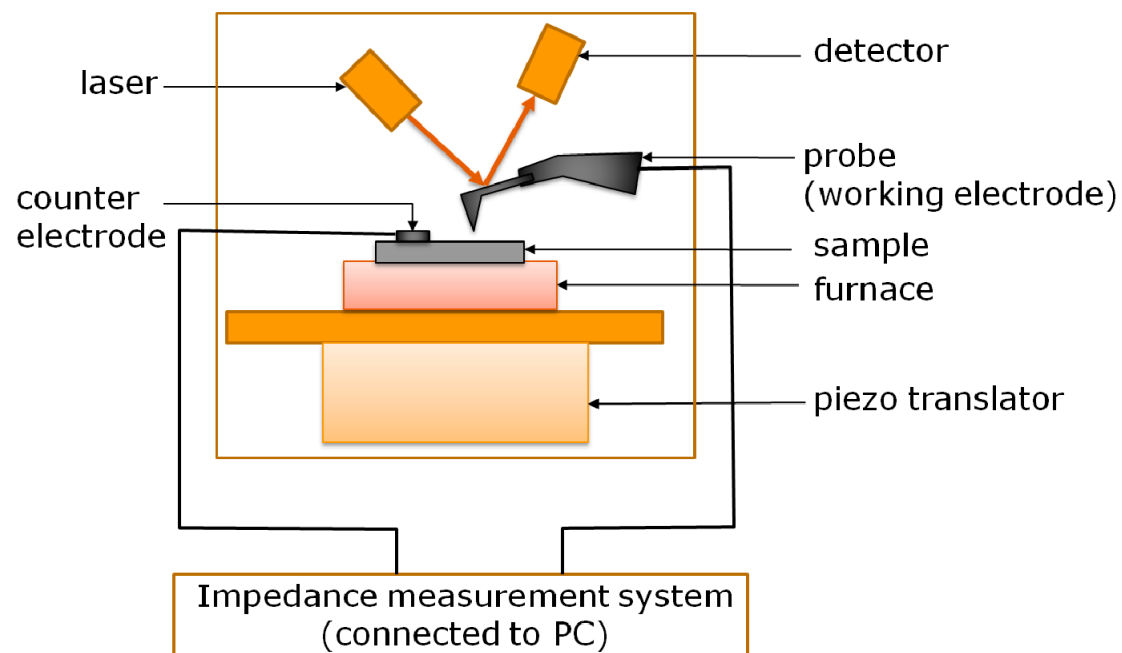
Typical use of thermal analysis @ Risø DTU

- **Dilatation, sintering shrinkage and profile characterisation, warping during processing**
- **Thermogravimetry and dilatometry with complex thermal profiles, eg:**
 - **Binder removal, sintering, thermal decomposition**
 - **Reactivity with different atmospheres,**
 - **Corrosion**
 - **Oxygen stoichiometry.**
- **Glass transition, crystallisation**
- **Determination of heat capacity, thermal conductivity, Seebeck coefficient**
- **High temperature XRD**

CAHT-SPM



Contact measurements
"Controlled atmosphere"
Up to 650-700°C

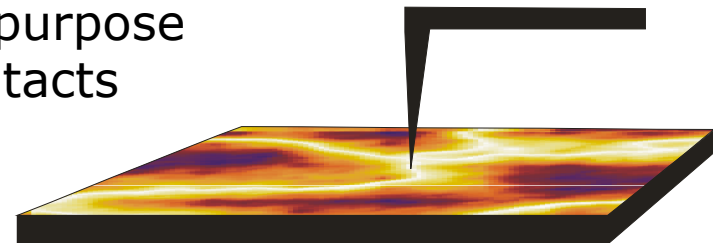


Contact and non contact measurements
Kelvin probe (surface potential)
Controlled atmosphere – pO_2 monitor
Up to 850°C

Purpose of the CAHT-SPM

We want to probe local electrochemical properties ($1 \mu\text{m}^2$ or smaller) in-situ in SOC electrode or other materials ($> 600^\circ\text{C}$) and in a controlled atmosphere

Custom made probes are essential for the purpose of the CAHT-SPM eg. for studying contacts between electrode materials

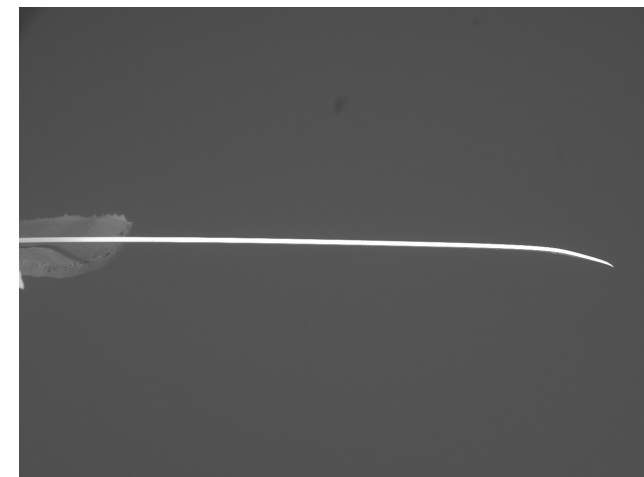


Probe properties

- Stable at high temperatures
- at reducing and oxidising conditions
- electrically conductive

At the moment, probes are from

- Ceramics: LSM/YSZ
- Platinum-iridium



0315-11c0001

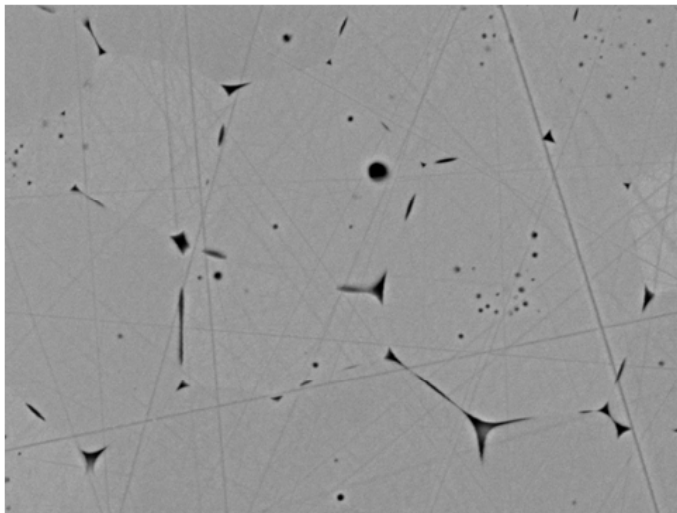
2010-03-26

L

x50

2 mm

Si impurities in YSZ grain boundaries

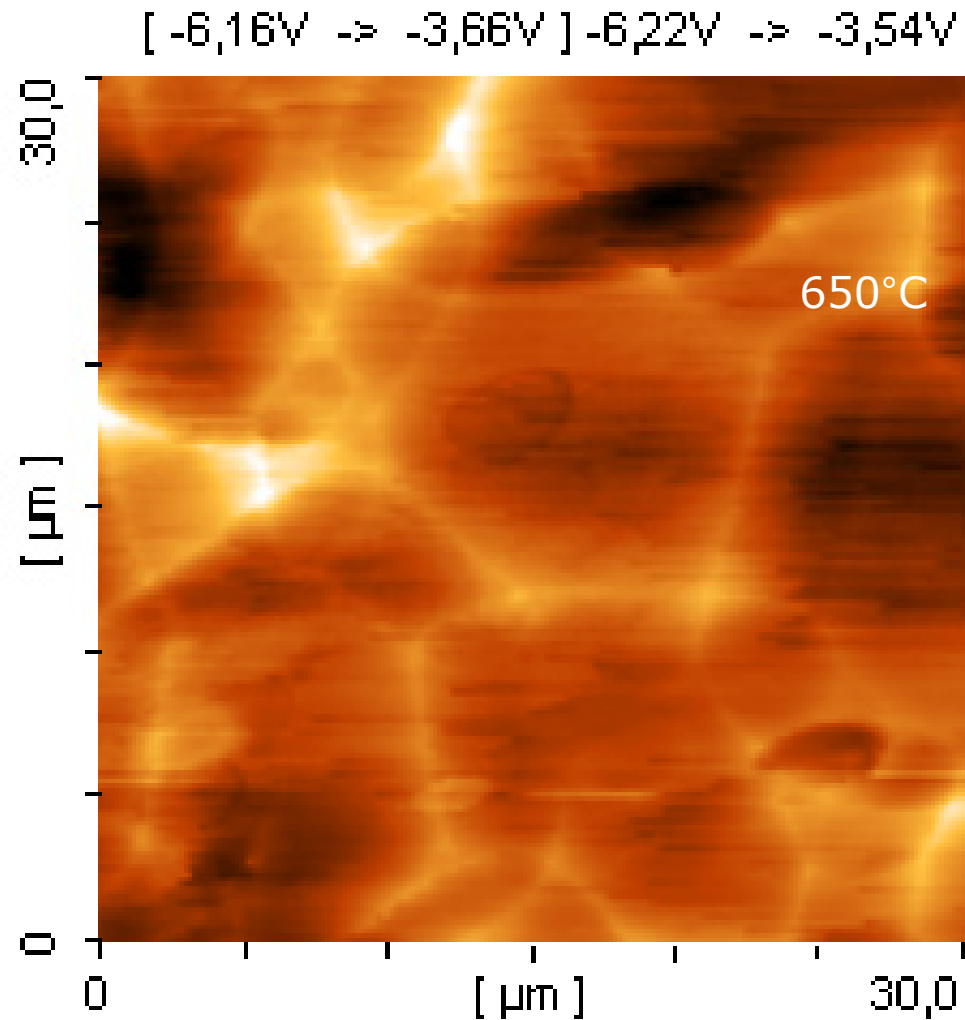


Si_YSZ_10001 2009-08-04 L x6,0k 10 μm

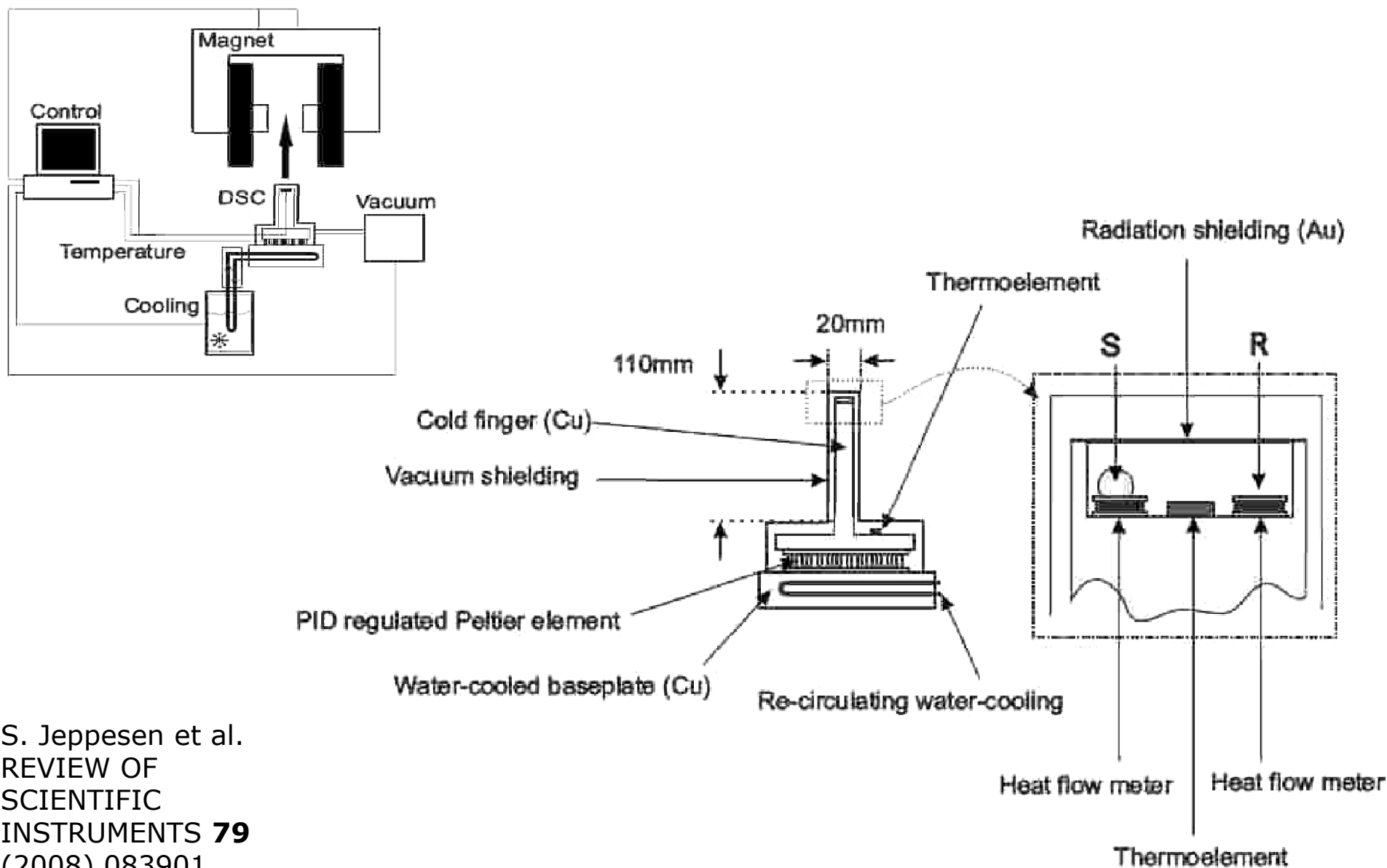
YSZ with 1000 ppm, sintered and polished

Dark = high conductivity,

White = low conductivity

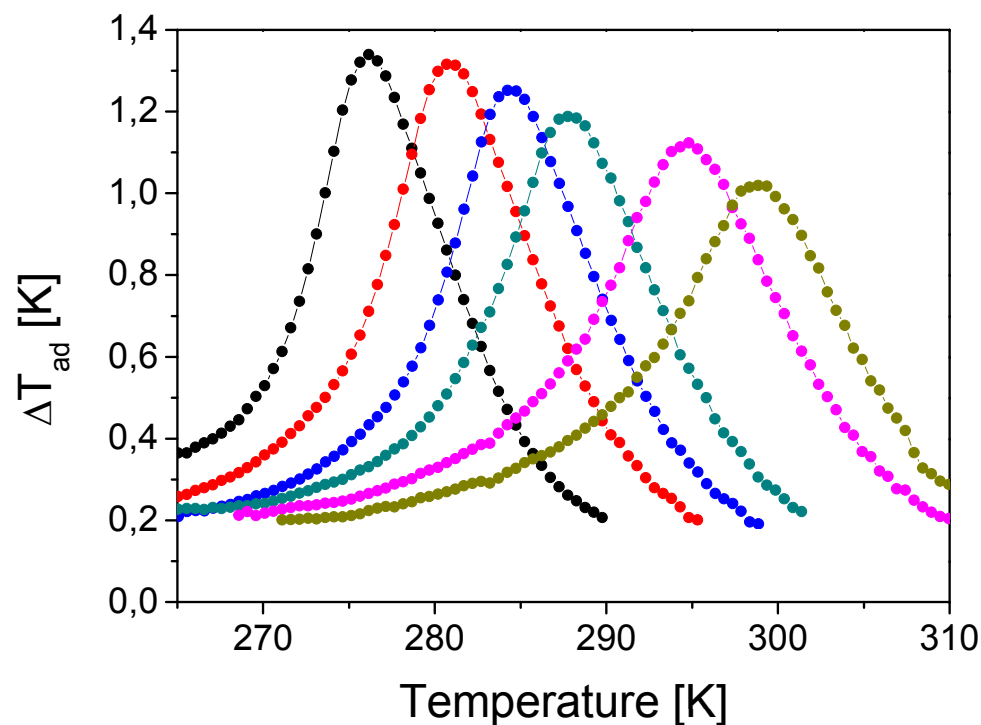
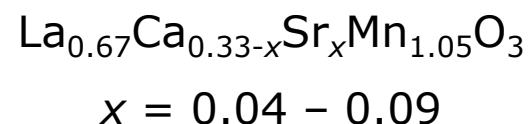
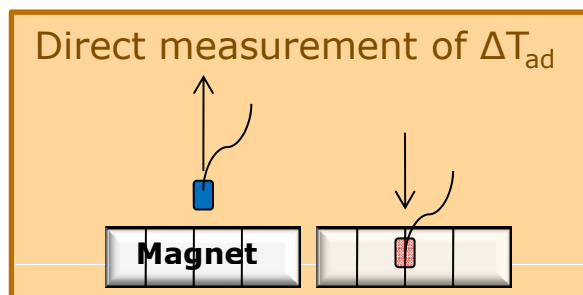


DSC for indirect measurement of the magnetocaloric effect



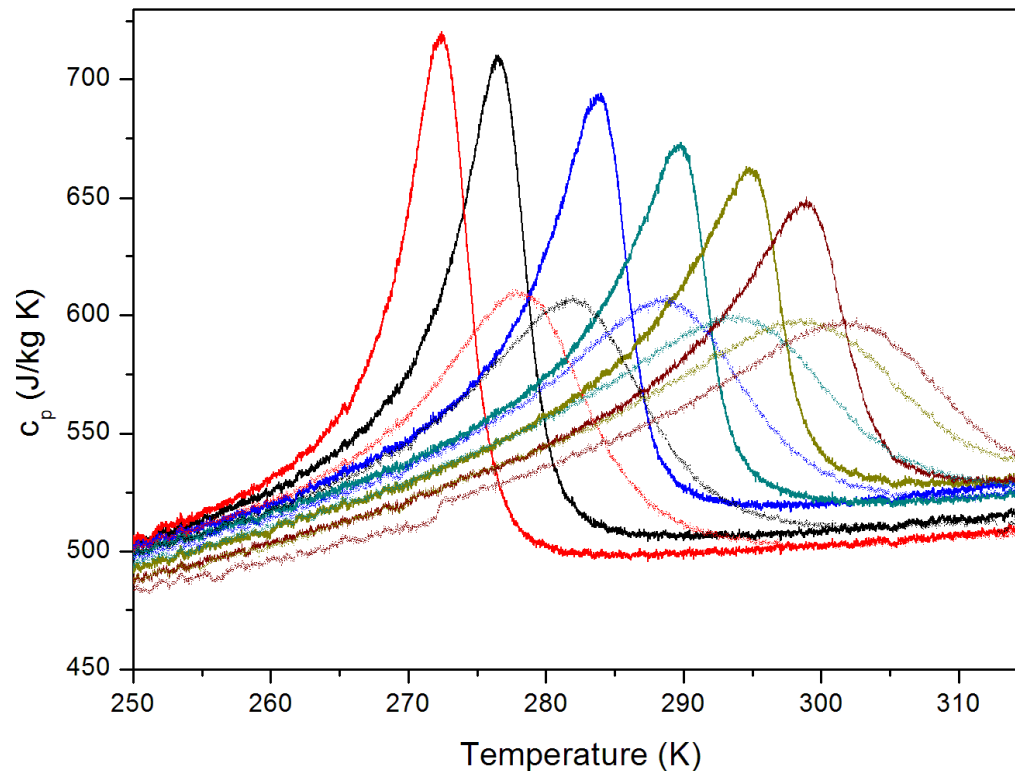
Perovskite manganites

- A series of manganites has been prepared, varying Ca/Sr.
- The Curie temperature can be controlled.
- ΔT_{ad} is the temperature change of the material when 1 T magnetic field is applied.
- It is measured directly



Specific heat of the perovskites

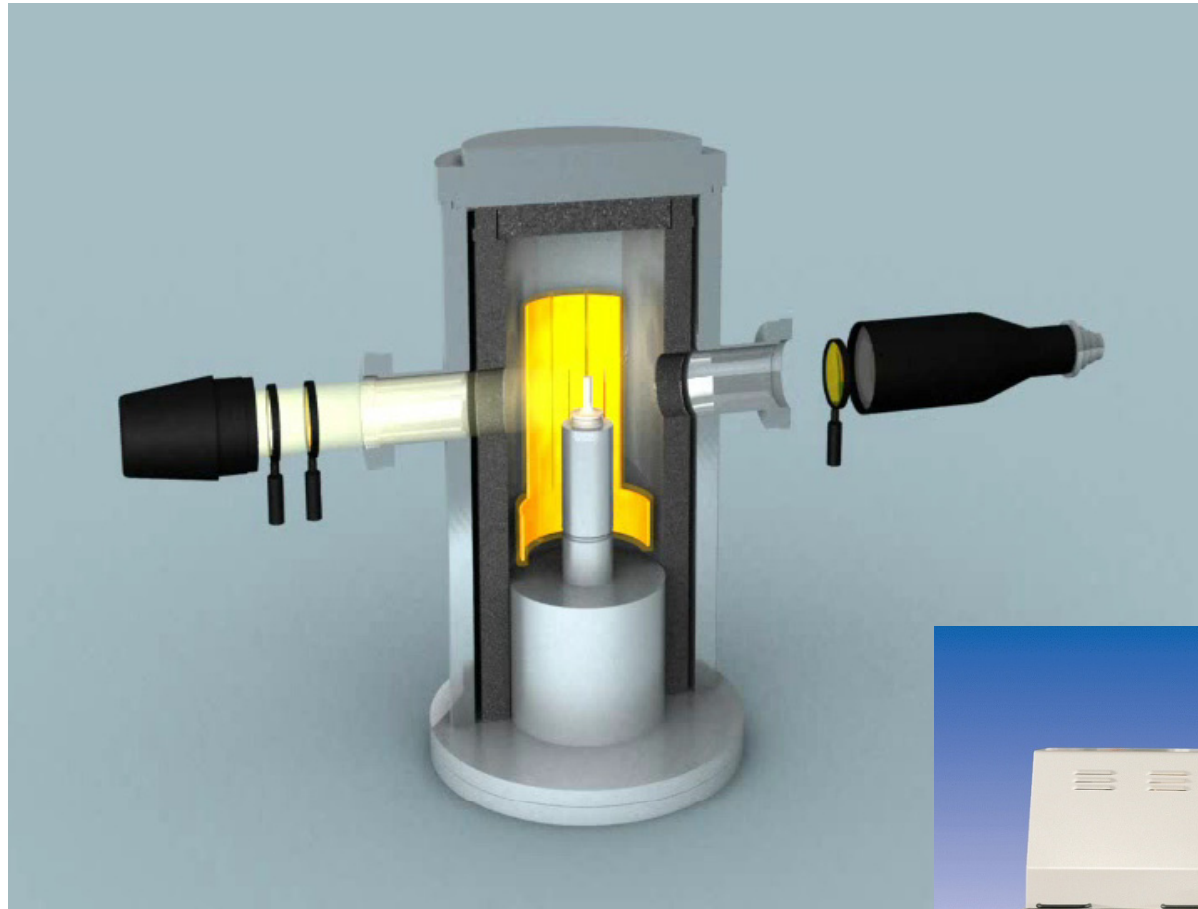
- Full lines are 0 T and dotted are 1 T magnetic field



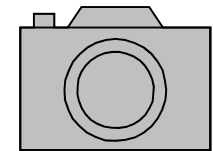
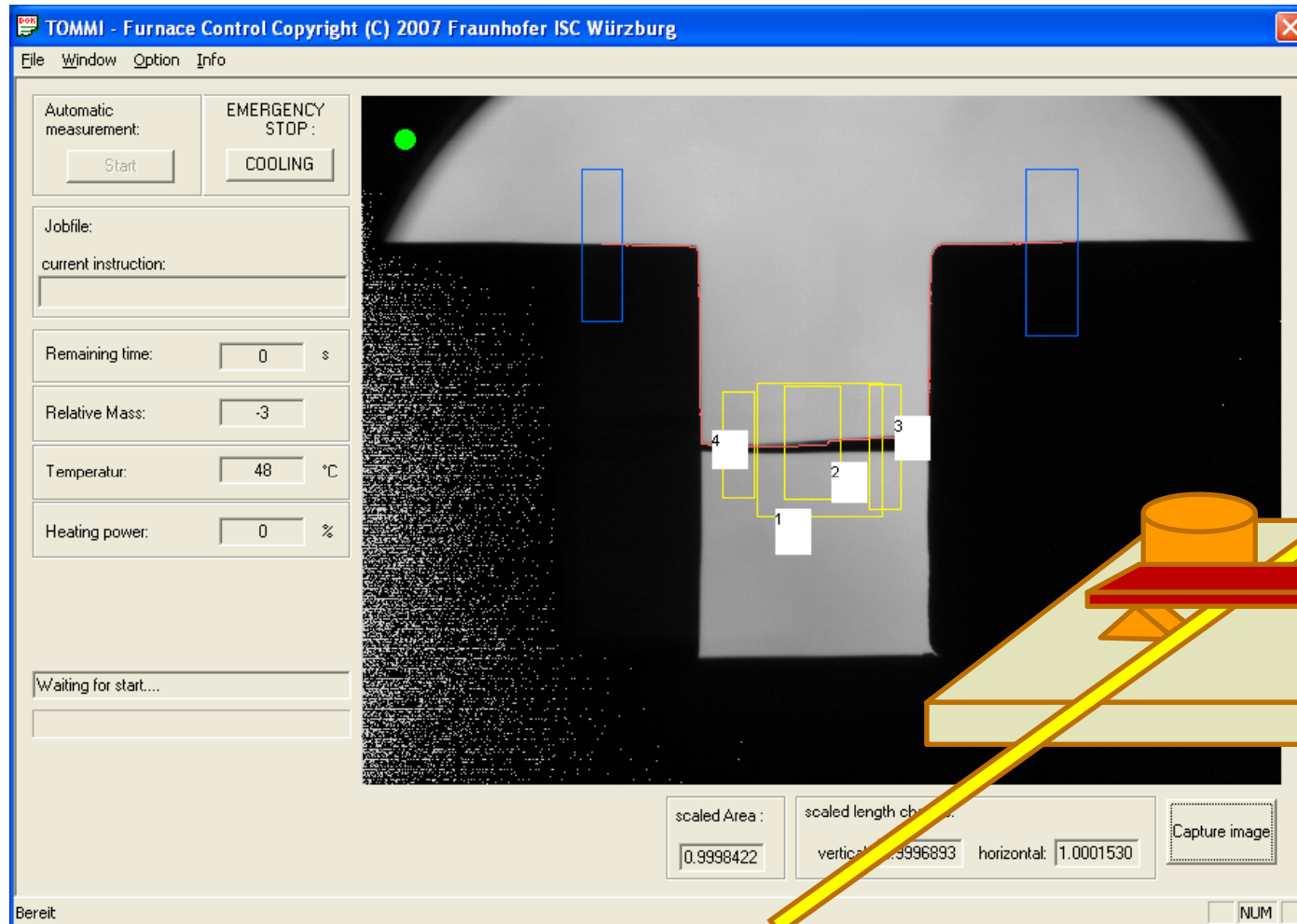
- The adiabatic temperature change (ΔT_{ad}) can be found directly or by measuring magnetisation (m) and specific heat (c_p) versus temperature (T) and magnetic field (H).

$$\Delta T_{\text{ad}} = -\mu_0 \int_{H_i}^{H_f} \frac{T}{c_p} \left(\frac{\partial m}{\partial T} \right)_H dH$$

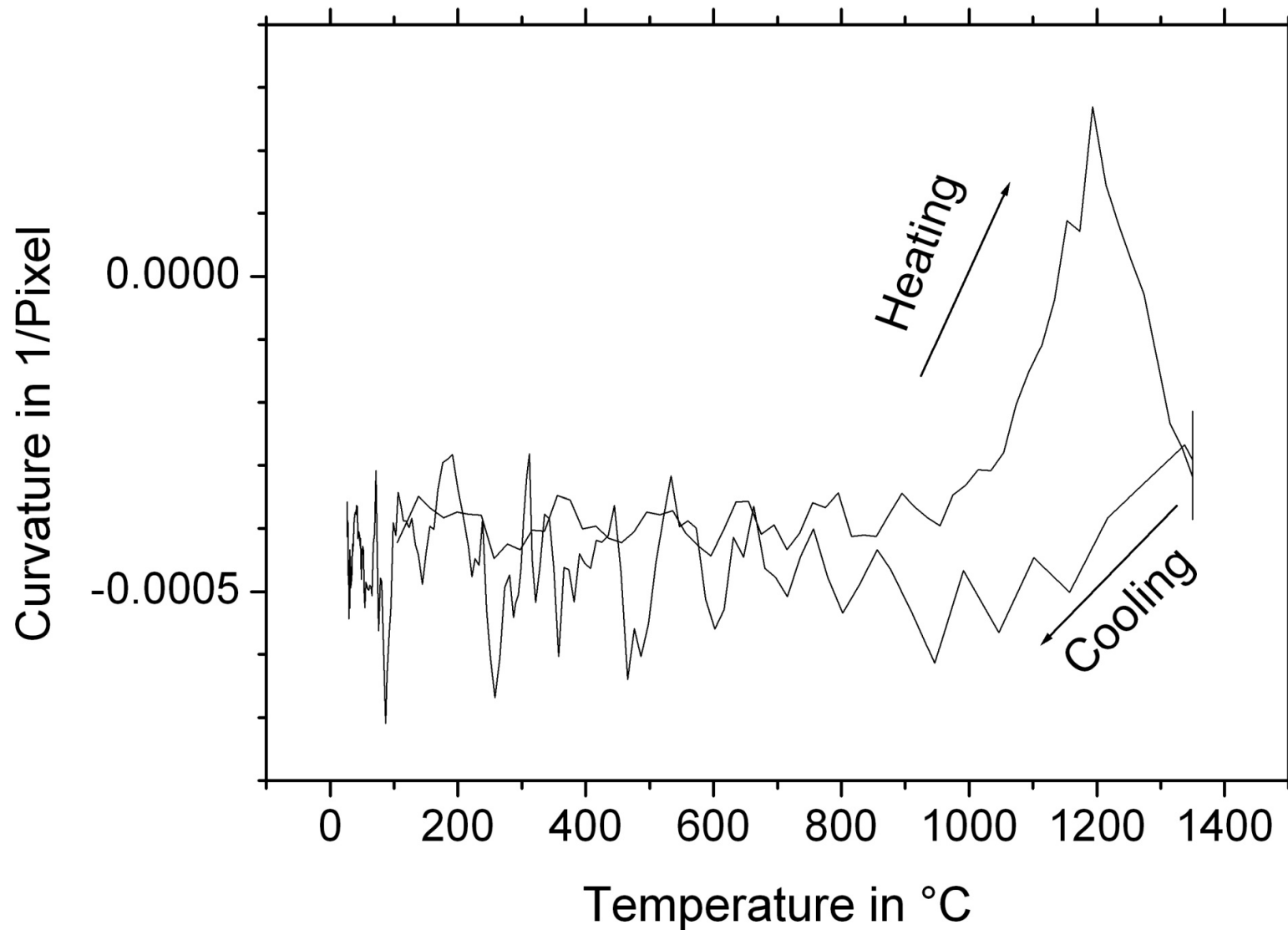
Optical dilatometer



Analysis set-up

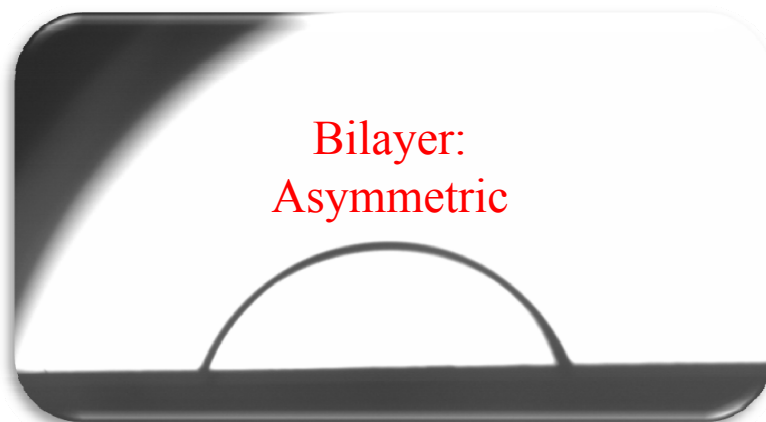


Bending during sintering a fuel cell

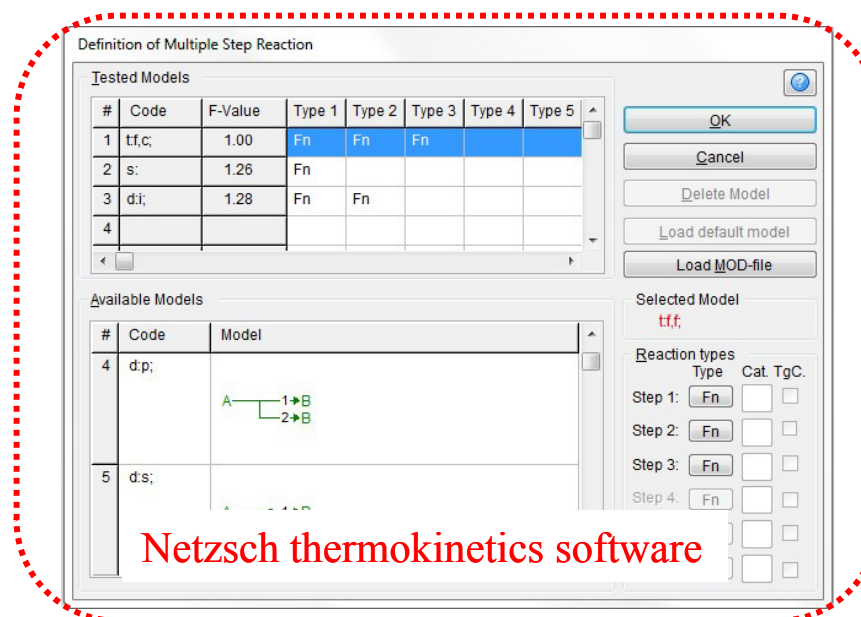
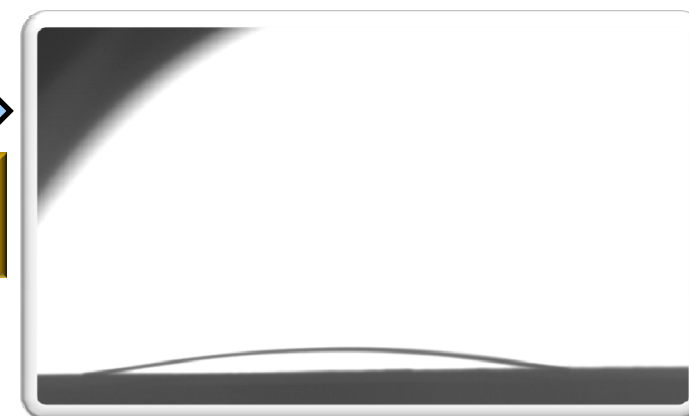
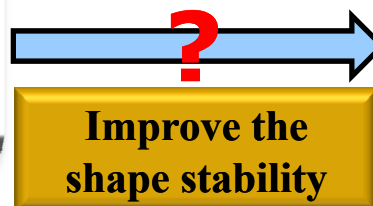


Optimization of a binder removal profile

The aim is to optimize binder removal- and sintering profiles in order to reduce warping of LSM/CGO bilayers. Processes are characterised through analysis of the kinetic field.



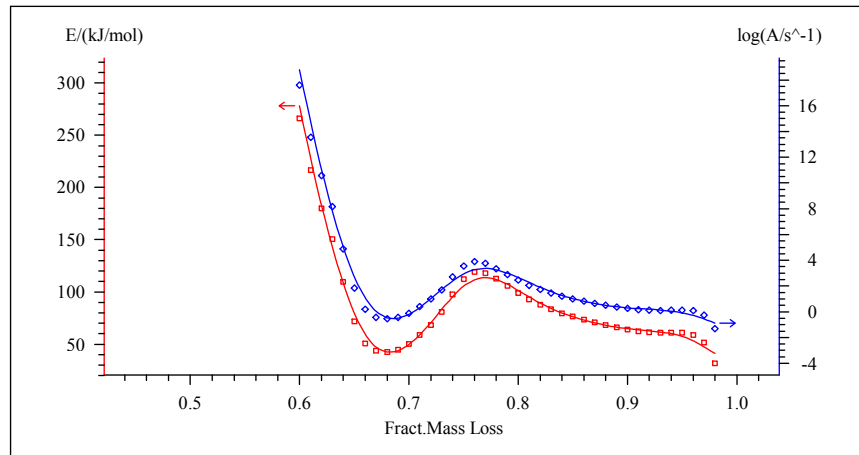
166°C



Binder removal thermokinetics analysis

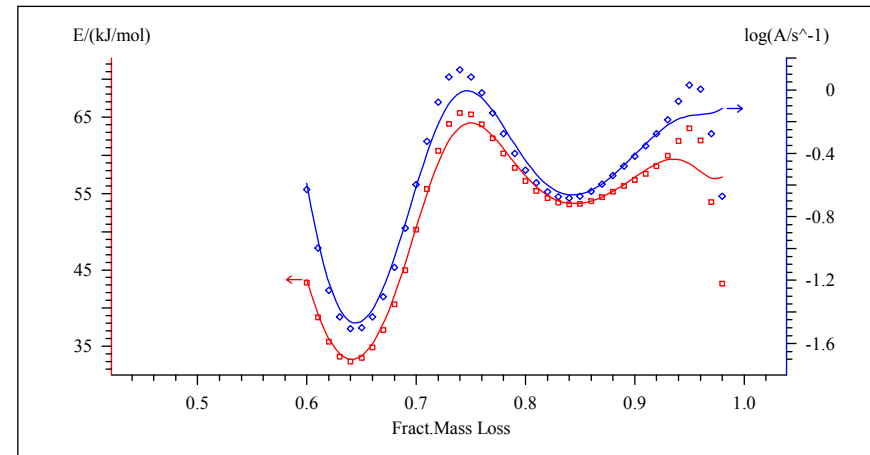
CGO Tapes:

Friedman Analysis CGO

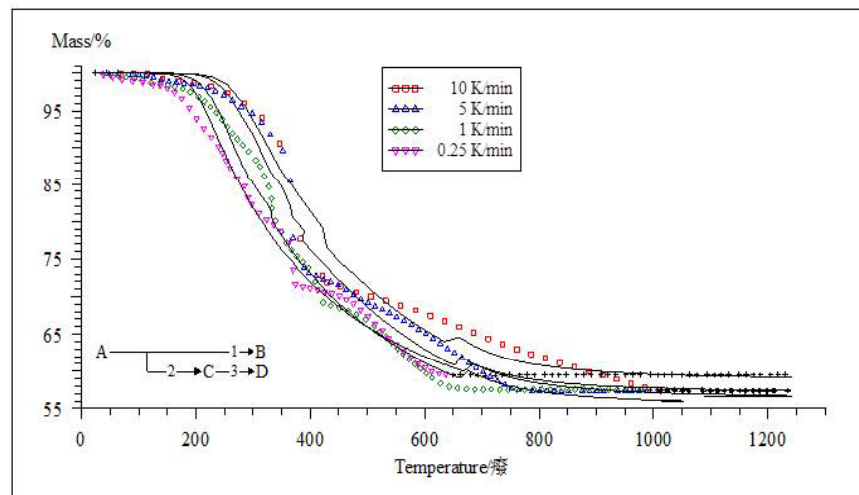


LSM/CGO Bilayer tapes:

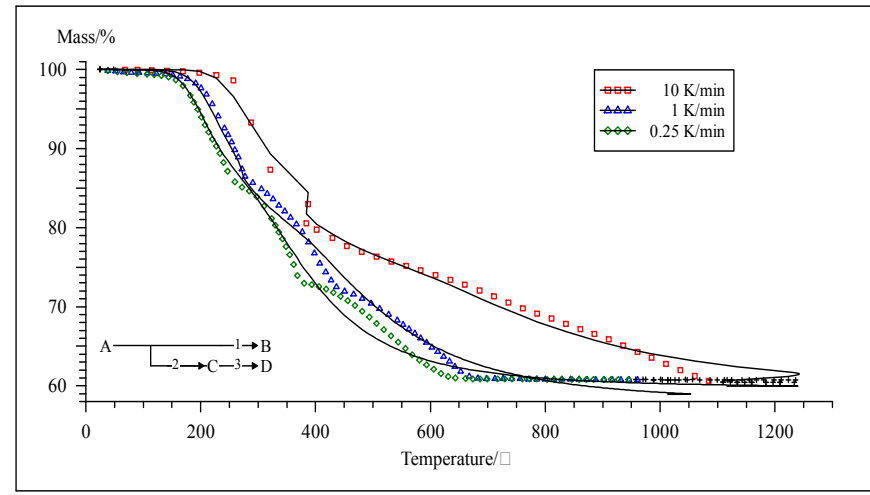
Friedman Analysis LSM/CGO



NETZSCH Thermokinetics CGO

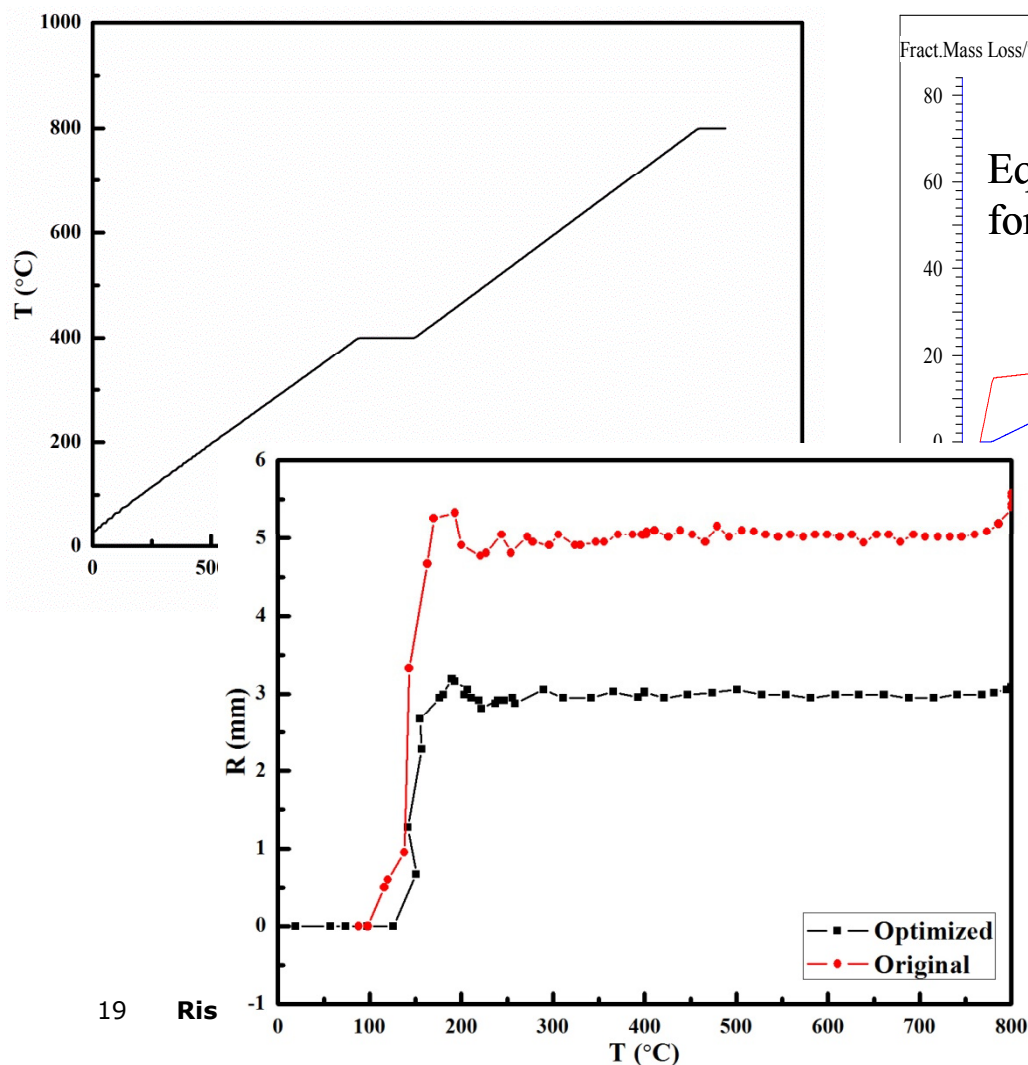


NETZSCH Thermokinetics LSM/CGO

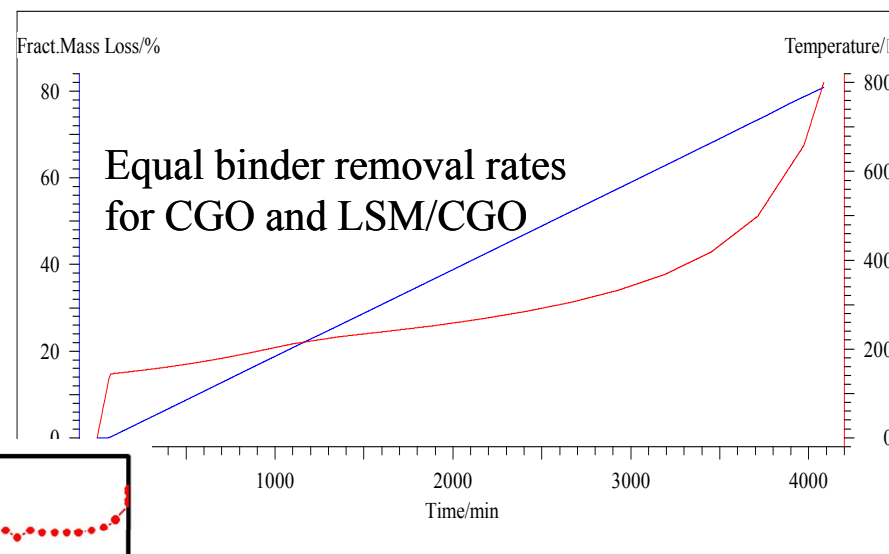


Binder removal profile improved

Original profile



Optimized profile



Original



Optimized



Sintering of CGO, $\text{Ce}_{0.9}\text{Gd}_{0.1}\text{O}_{1.95-\delta}$

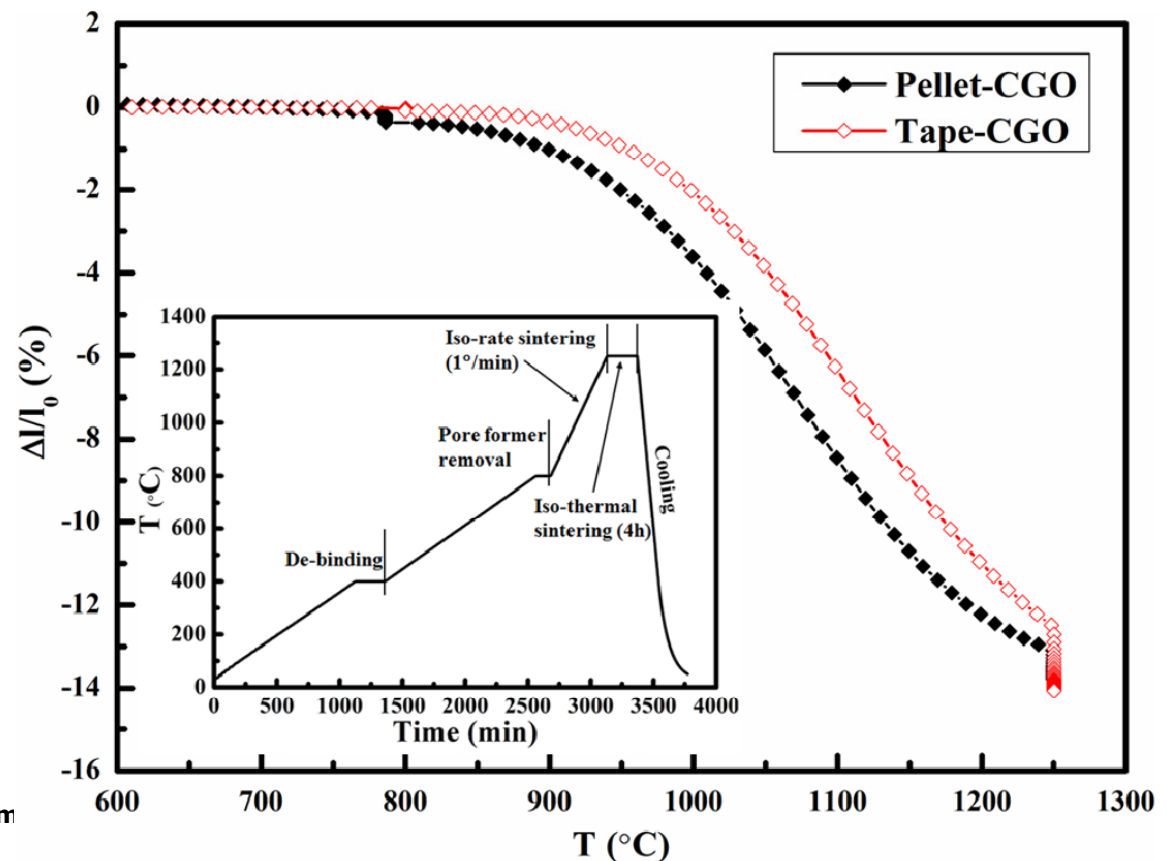
Scope is to study the densification behaviour of powder from two different processing methods – tape casting and dry pressing – as well as addition of sintering aids to control sintering behaviour:

For the same composition, the densification behaviour is different between dry pressing pellets and tape casting layers.

Green density:

Tape cast: ~40%TD

Dry pressed: ~50%TD



Theoretical approach:

I. Iso-conversion lines:

$$\dot{\rho} = \frac{A}{RT} \exp\left(\frac{-Q_d}{RT}\right) f(\rho, d) \quad \ln(\dot{\rho} T) = \frac{-Q_d}{RT} + \ln \frac{A}{R} + \ln f(\rho, d)$$

$$\ln\left(-\frac{dl}{dt} T\right) = \frac{-Q_l}{RT} + \ln \frac{C}{R} + \ln f(l, d)$$

II. Master Sintering Curve (MSC):

$$\frac{d\rho}{3\rho dt} = \frac{\gamma \Omega(\Gamma(\rho)) D_0}{kT (G(\rho))^n} \exp\left(-\frac{Q}{RT}\right) \quad \Theta(t, T(t)) \equiv \int_0^t \frac{1}{T} \exp\left(-\frac{Q}{RT}\right) dt$$

Sintering at
different
heating rates



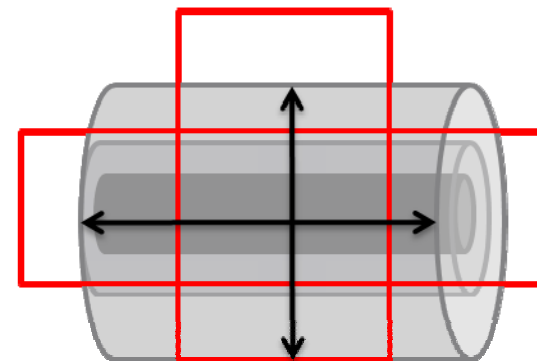
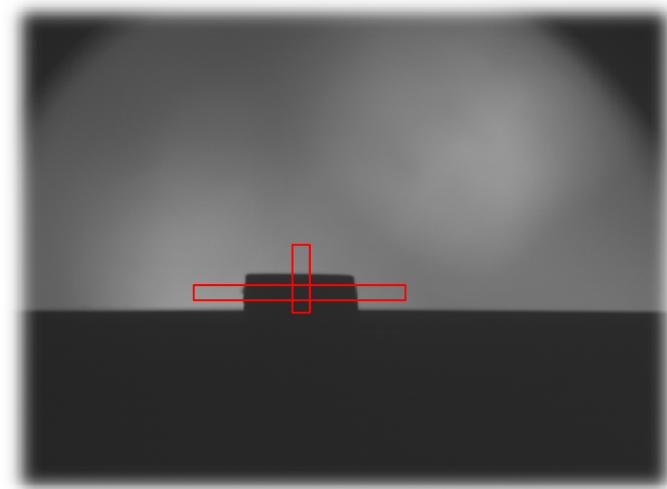
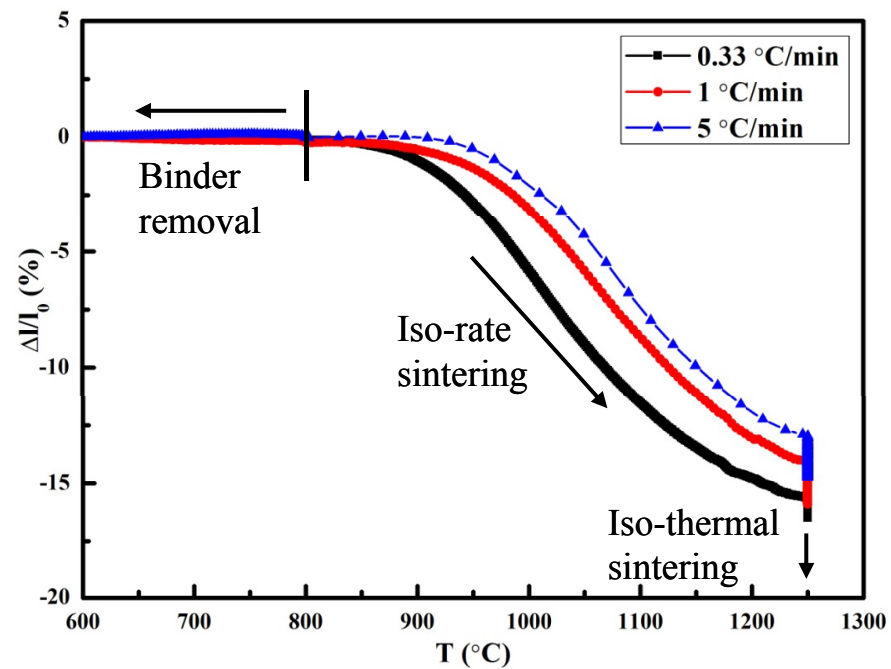
Activation
energy (Q)

III. Dorn's method

Step-wise isothermal heating

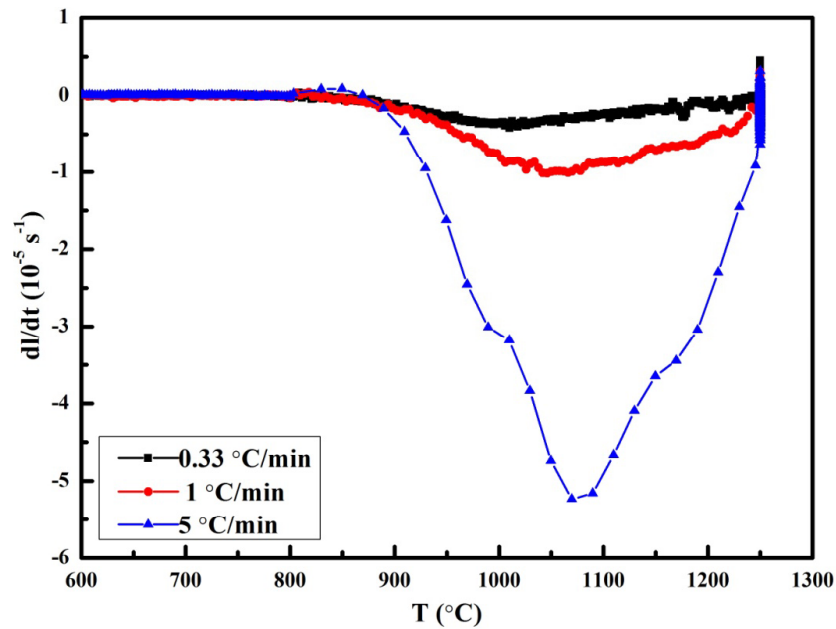
Densification at different heating rates

Shrinkage of CGO-tape



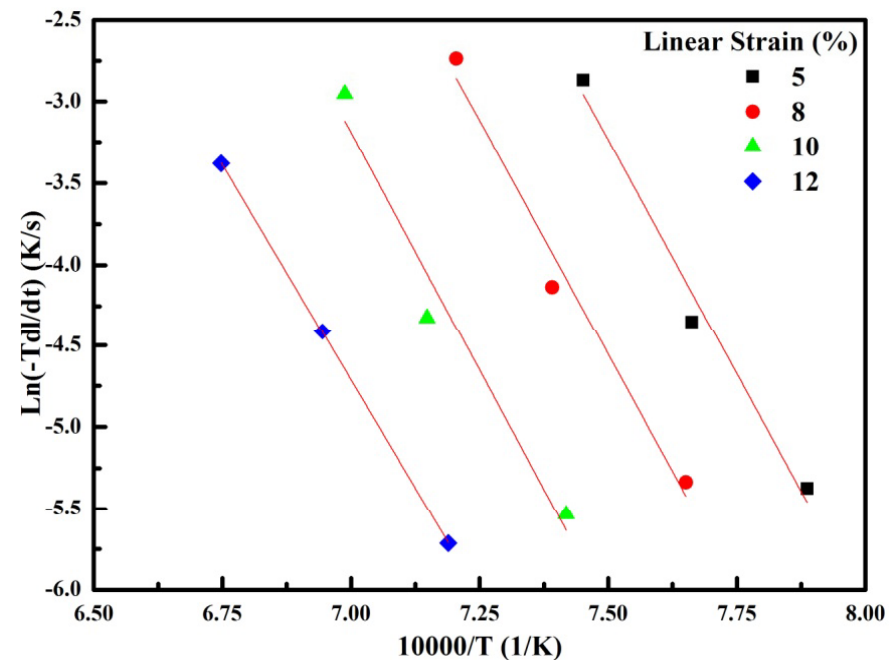
Activation energy

Determined by iso-conversion lines (sintering strain)



$$E_{\text{CGO}} = 440 \sim 485 \text{ kJ/mol}$$

$$\ln\left(-\frac{dl}{dt}T\right) = \frac{-Q_l}{RT} + \ln\frac{C}{R} + \ln f(l, d)$$

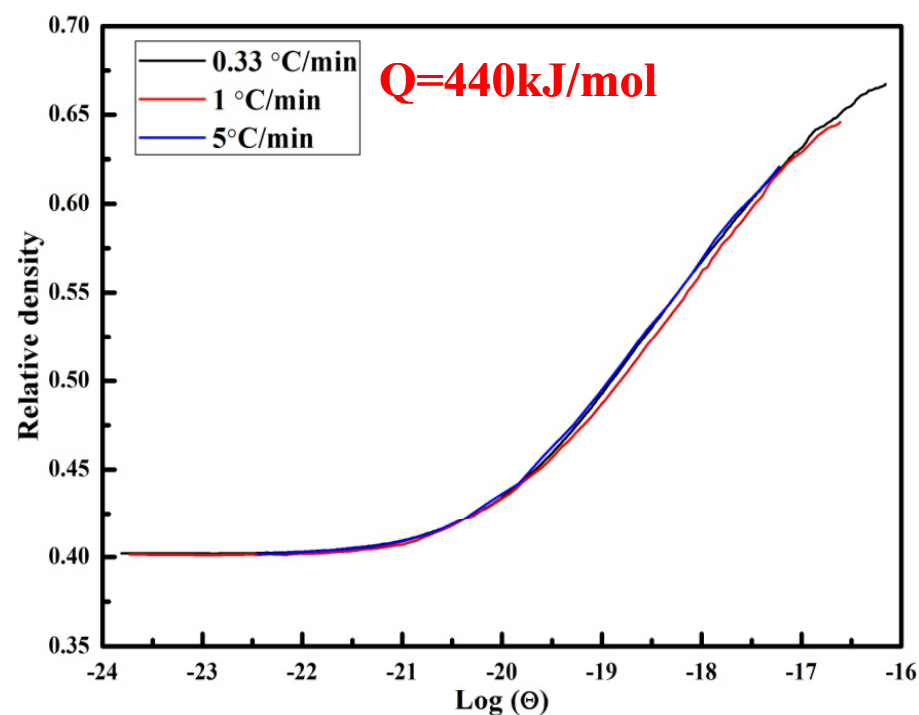
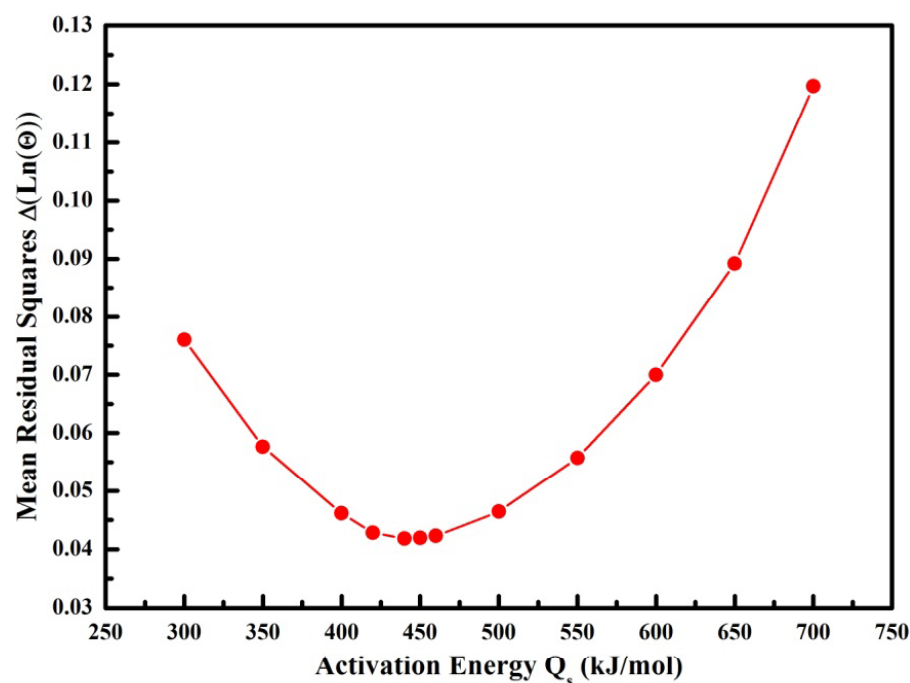


Activation energy determined by MSC

Mean Residual Squares:

$$MRS = \sqrt{\frac{1}{\rho_f - \rho_0} \int_{\rho_0}^{\rho_f} \frac{\sum_{i=1}^N ((\Theta_i / \Theta_{avg}) - 1)^2}{N} d\rho}$$

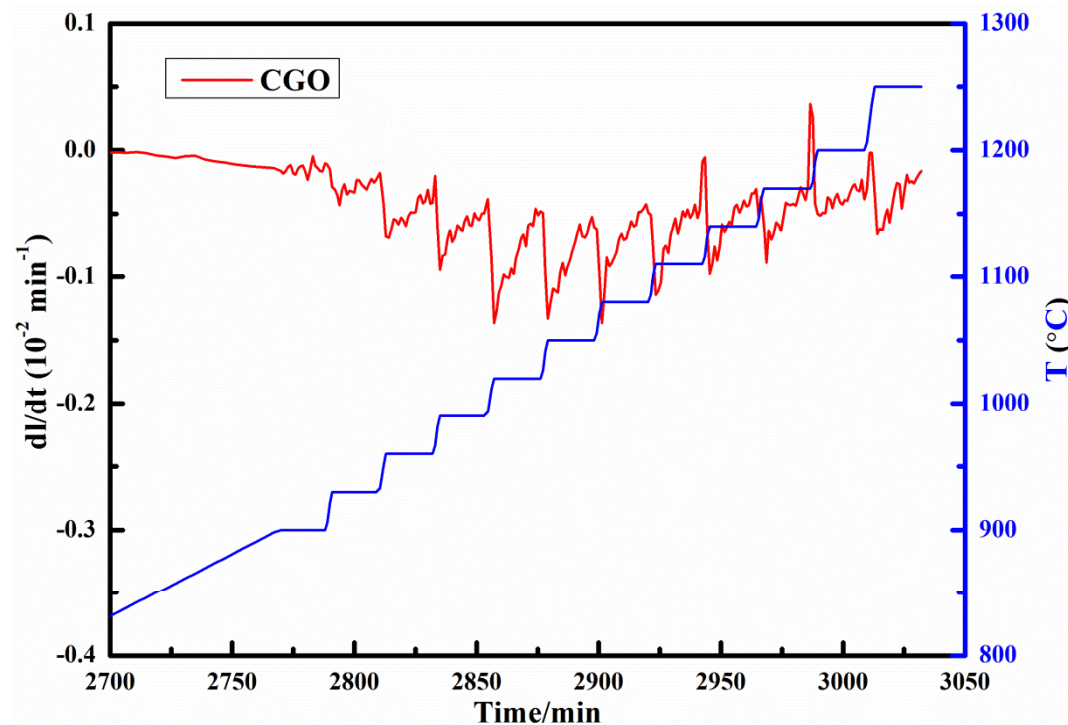
$$\Theta(t, T(t)) \equiv \int_0^t \frac{1}{T} \exp\left(-\frac{Q}{RT}\right) dt$$



Activation energy determined by Dorn's method:

$$v = \frac{d(\Delta l/l_0)}{dt} = k(T) \frac{(\Delta l/l_0)^{1-n}}{n}$$

$$Q = \frac{RT_1 T_2}{T_2 - T_1} \ln \left(\frac{T_2 v_2}{T_1 v_1} \right)$$



Activation energy (kJ/mol):

T(°C)	930	960	990	1020	1050	1080	1110
CGO	422	459	471	468	499	417	451

Activation energy via different methods

Iso-conversion lines method:

Shrinkage (%)	5	8	10	12
CGO (kJ/mol)	478	477	486	439

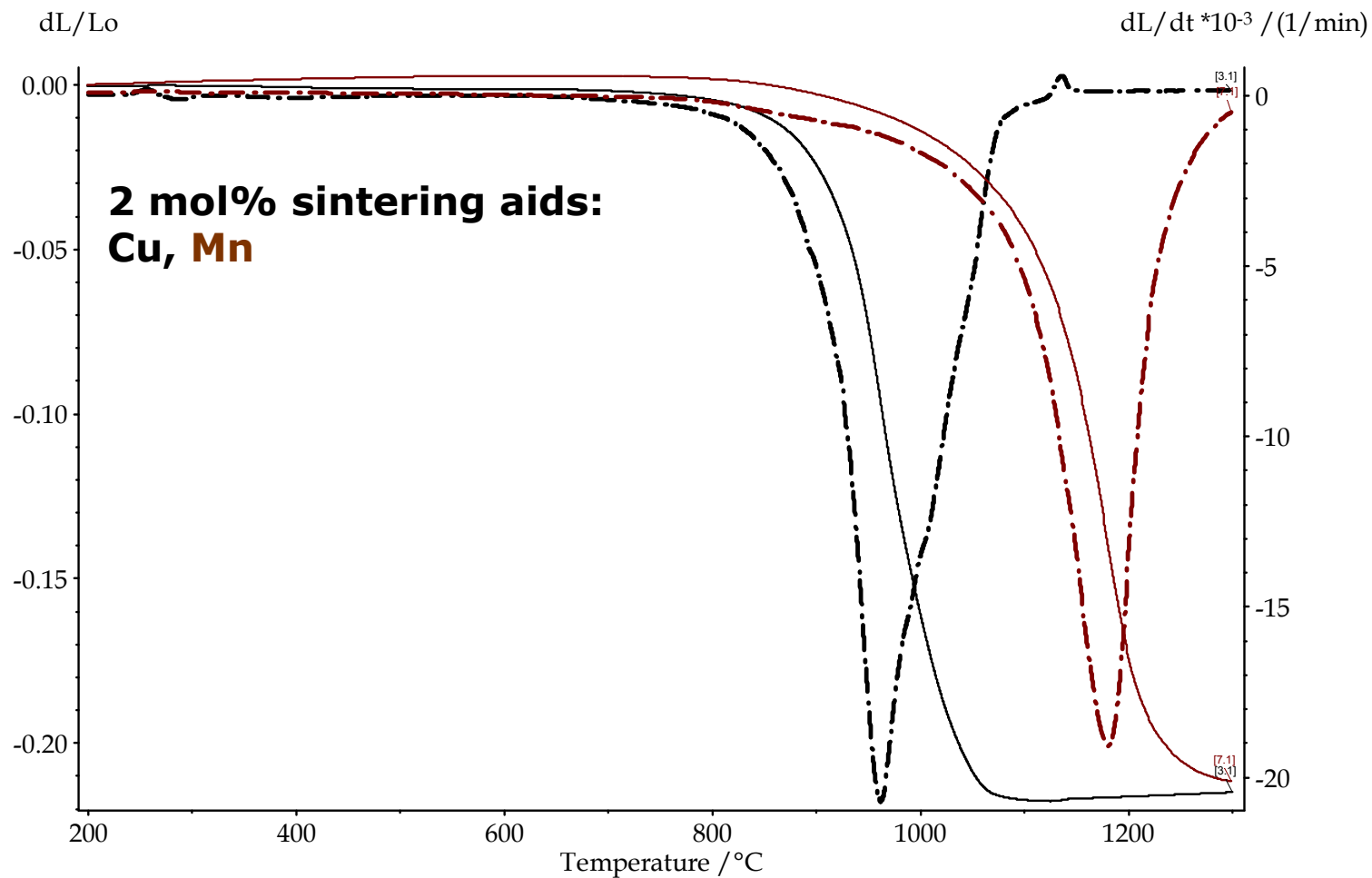
Master sintering curve:

Relative density	Full range
CGO (kJ/mol)	440

Dorn's method:

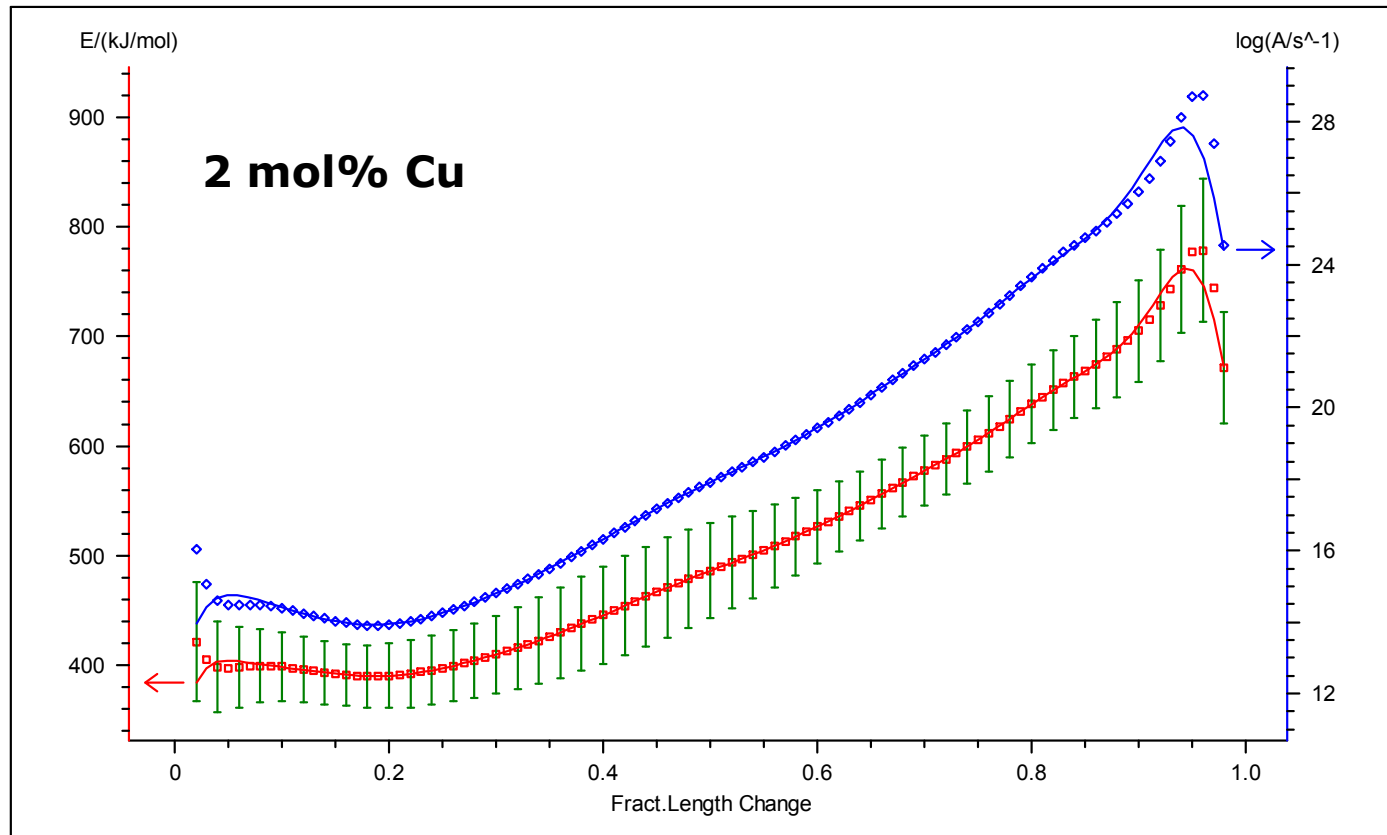
T(°C)	930	960	990	1020	1050	1080	1110
CGO (kJ/mol)	422	459	471	468	499	417	451

Sintering aids to control shrinkage

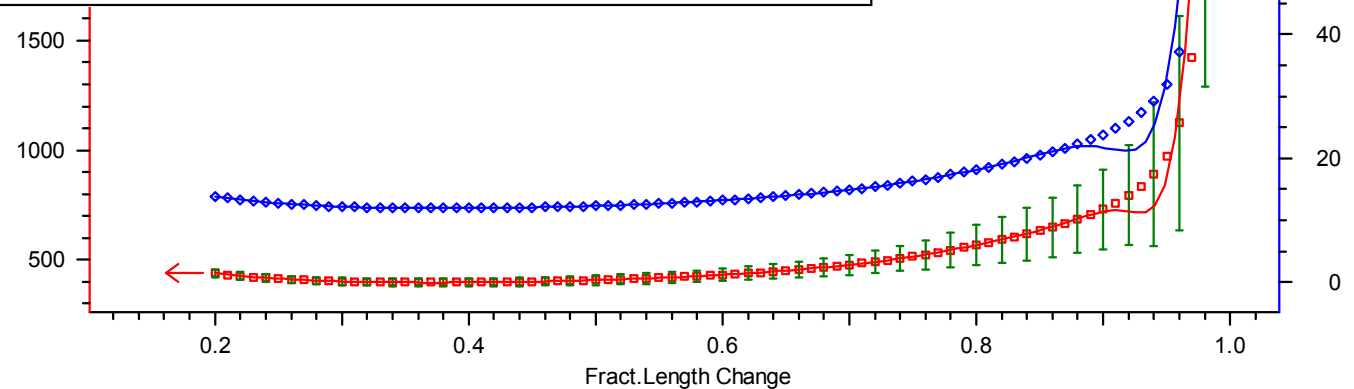


Activation energy by iso-conversion lines

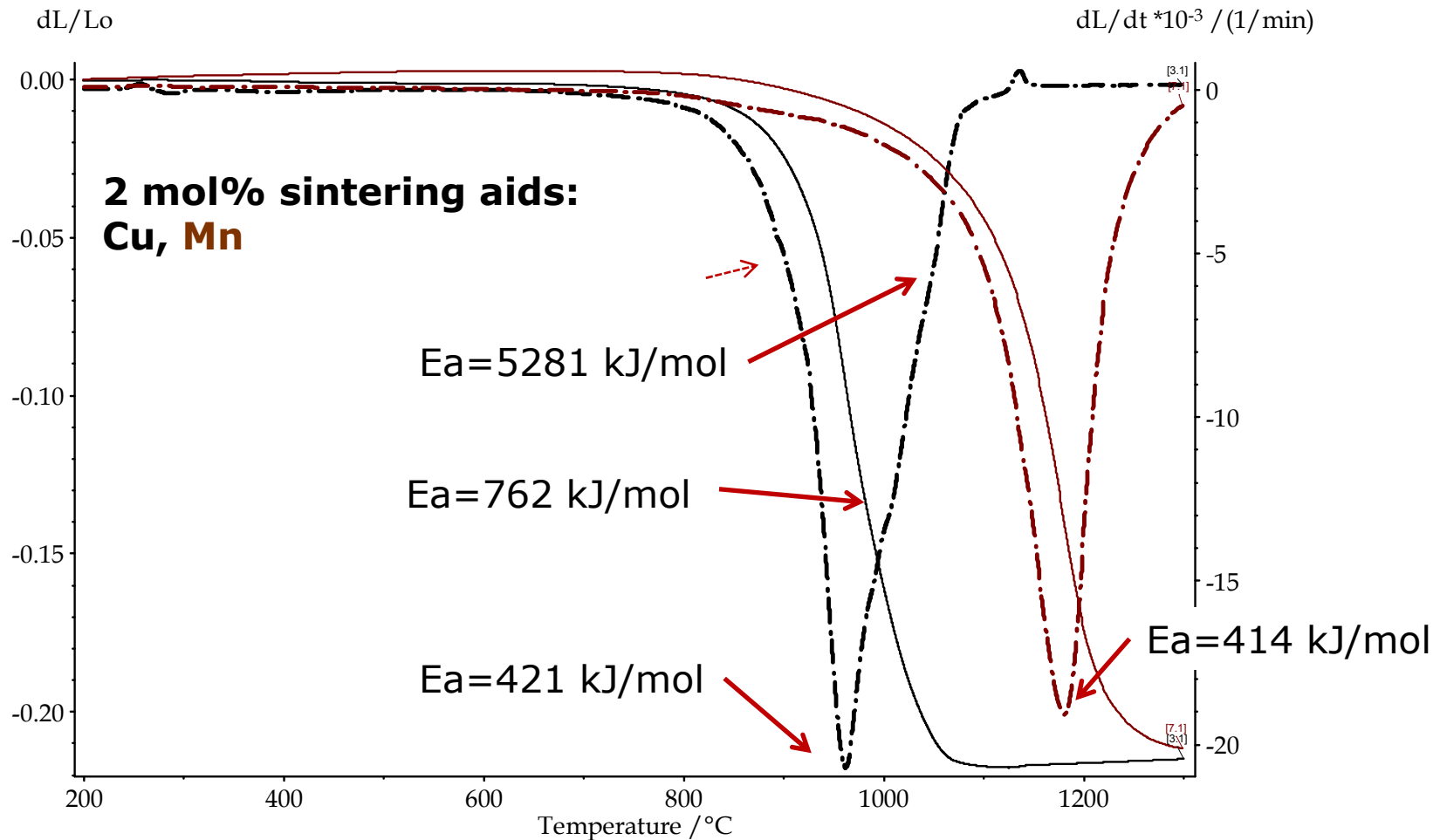
Friedman Analysis



2 mol% Mn



Activation energy for CGO with sintering aids

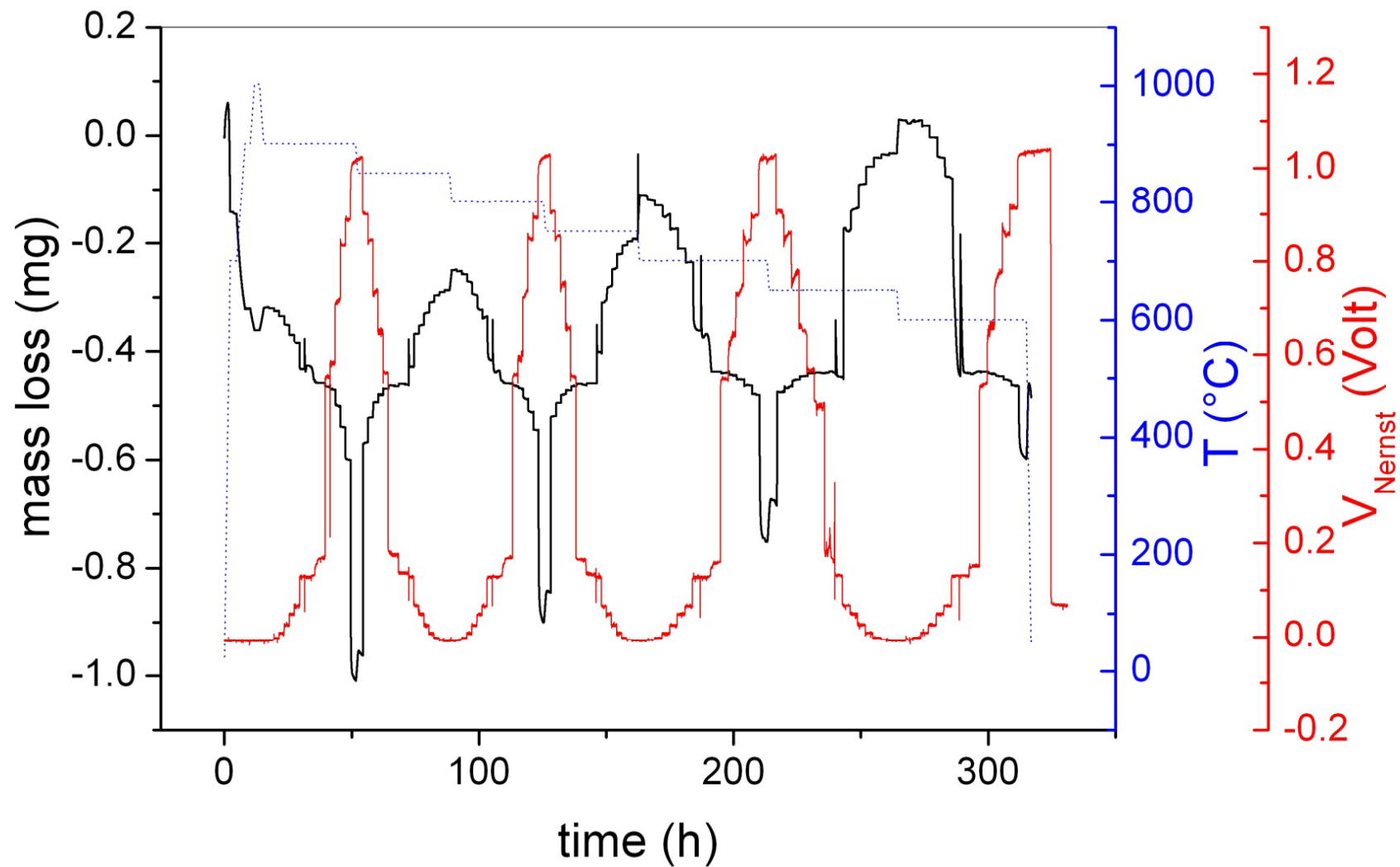


Studying gas-solid reactions



The symmetrical furnace design of the TG439 facilitates the running of longer and complicated heating- and gas-profiles, as it is not necessary to run a baseline.

The sample sizes are small and the balance sensitivity high, hence perfect for studying gas-solid reactions.



Weight change of $\text{Ce}_{0.8}\text{Pr}_{0.2}\text{O}_{2-\delta}$ as a function of T , $P_{\text{O}_2}(V_{\text{Nernst}})$

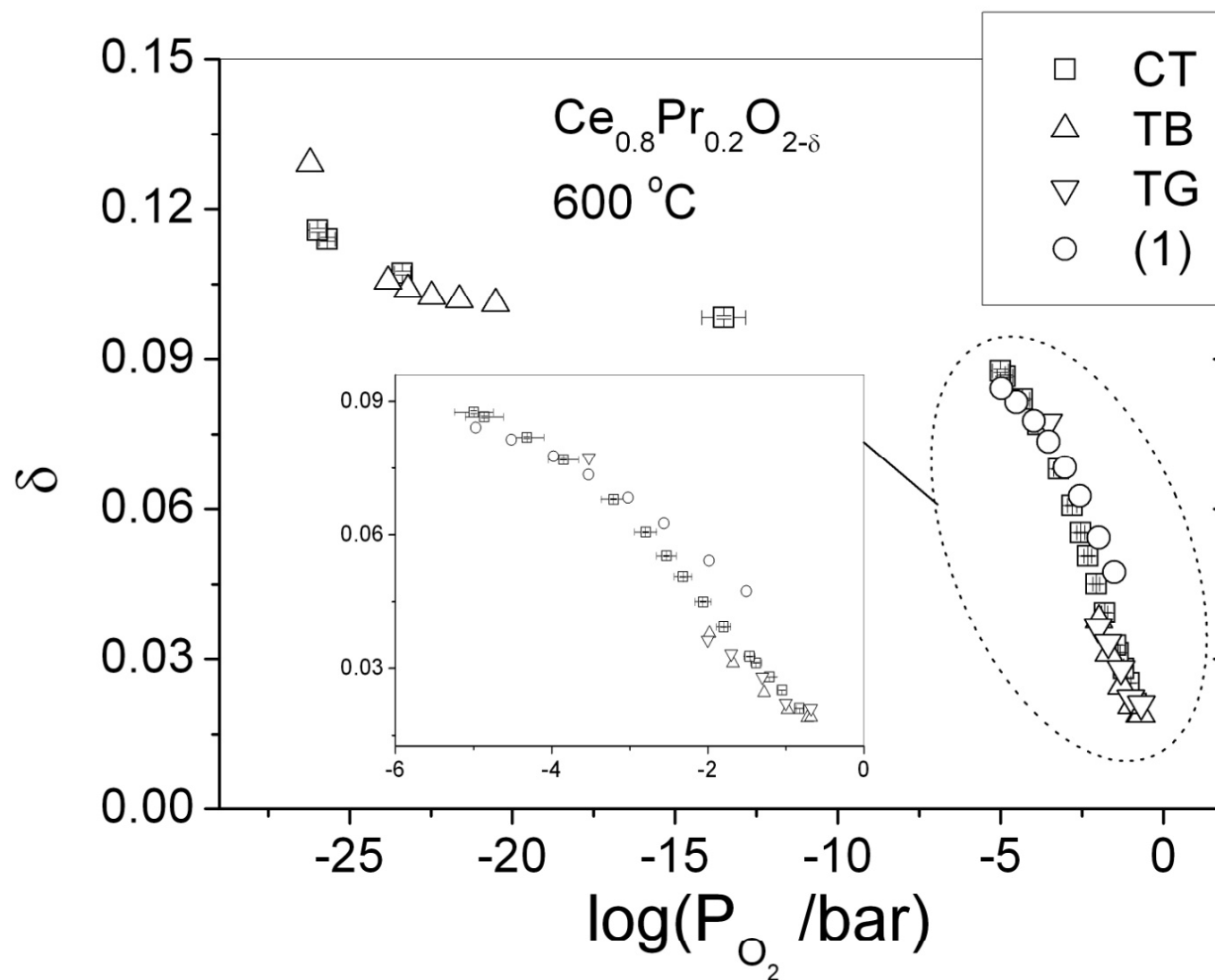
Netzsch TG439



Netzsch STA 409CD

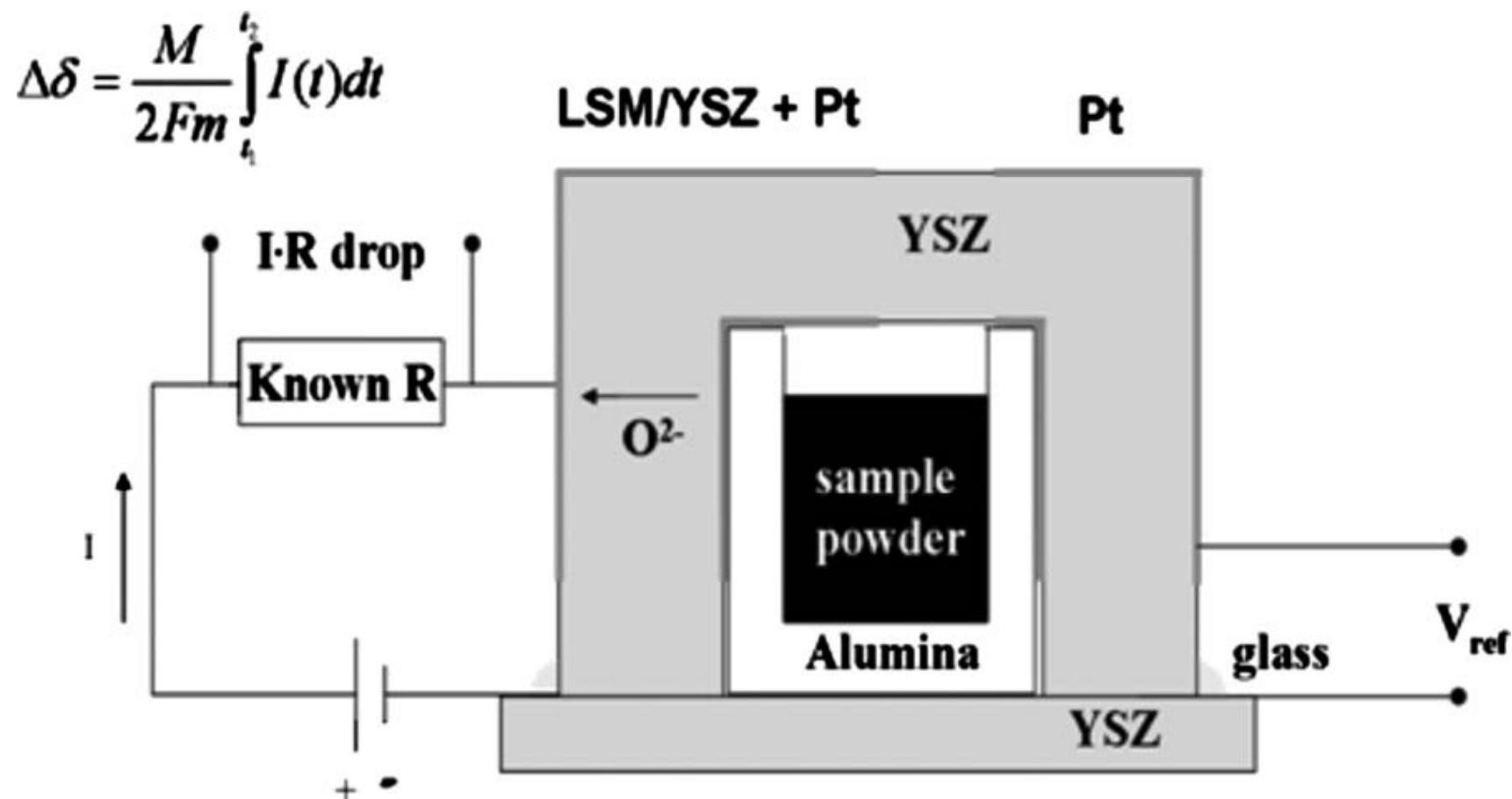


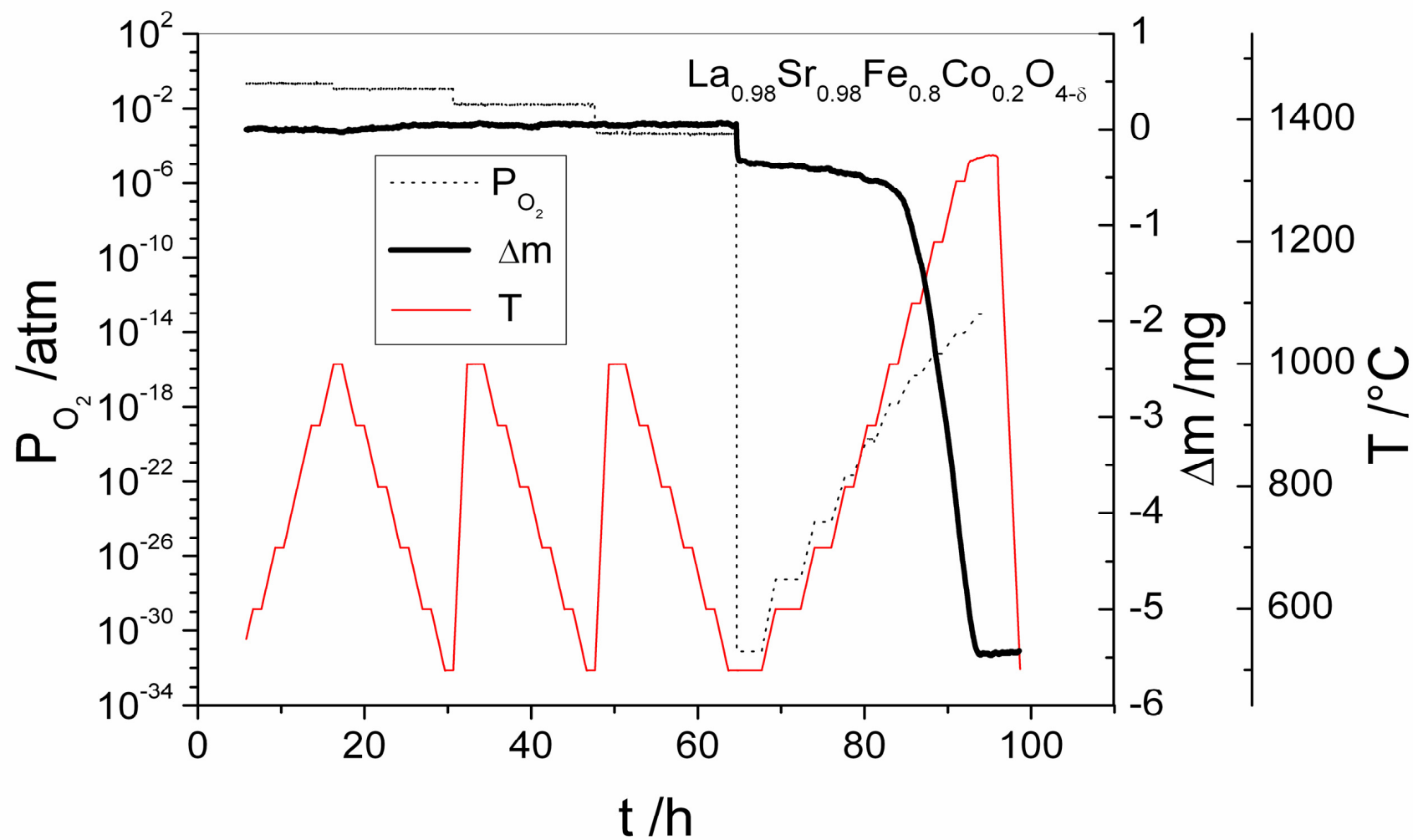
Oxygen nonstoichiometry – $\text{Ce}_{0.8}\text{Pr}_{0.2}\text{O}_{2-\delta}$ (CPO20)

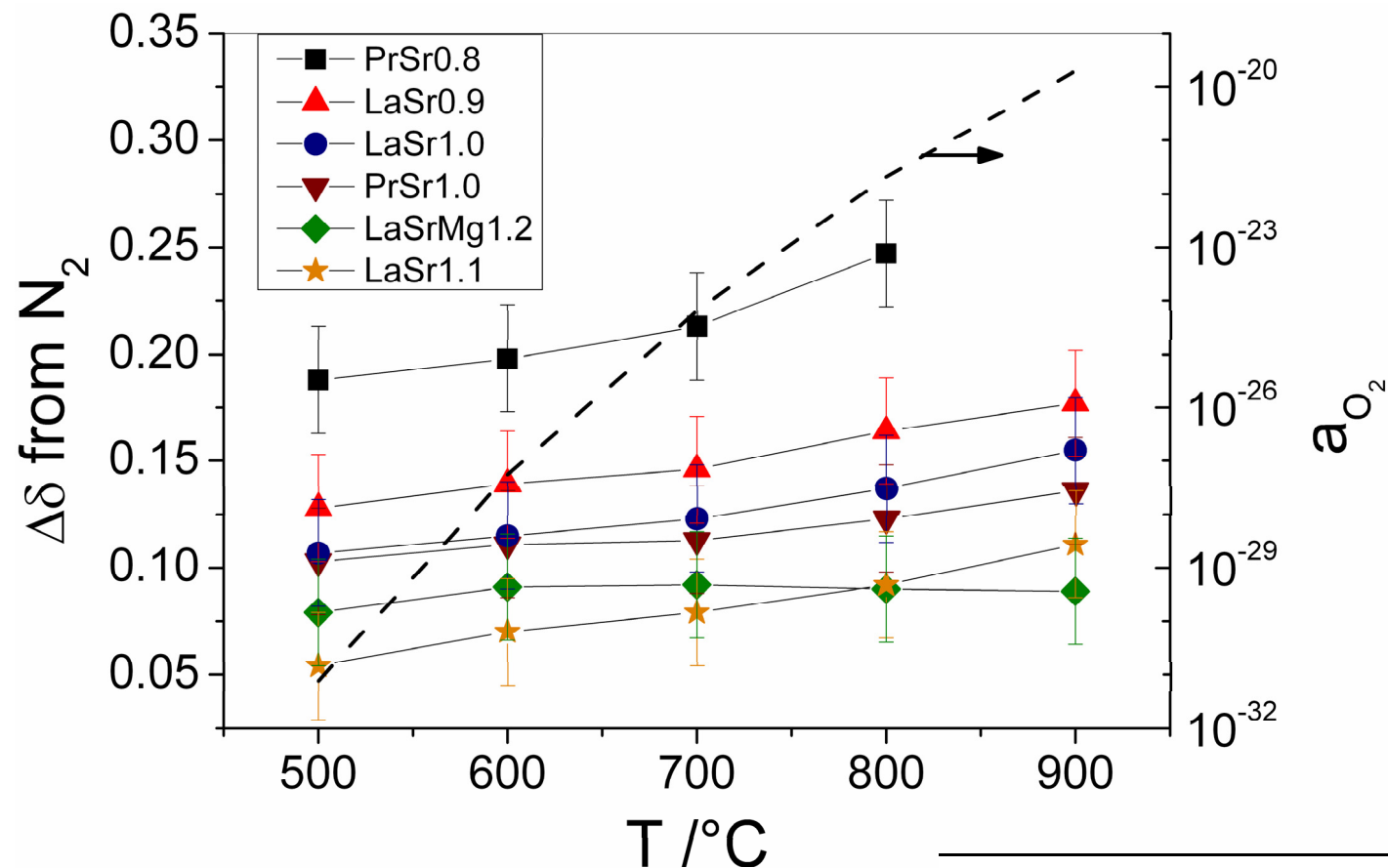


(1) T. S. Stefanik and H. L. Tuller, *J. Electroceram.*, **13**, 799 (2004).

Experimental setup used for coulometric titration



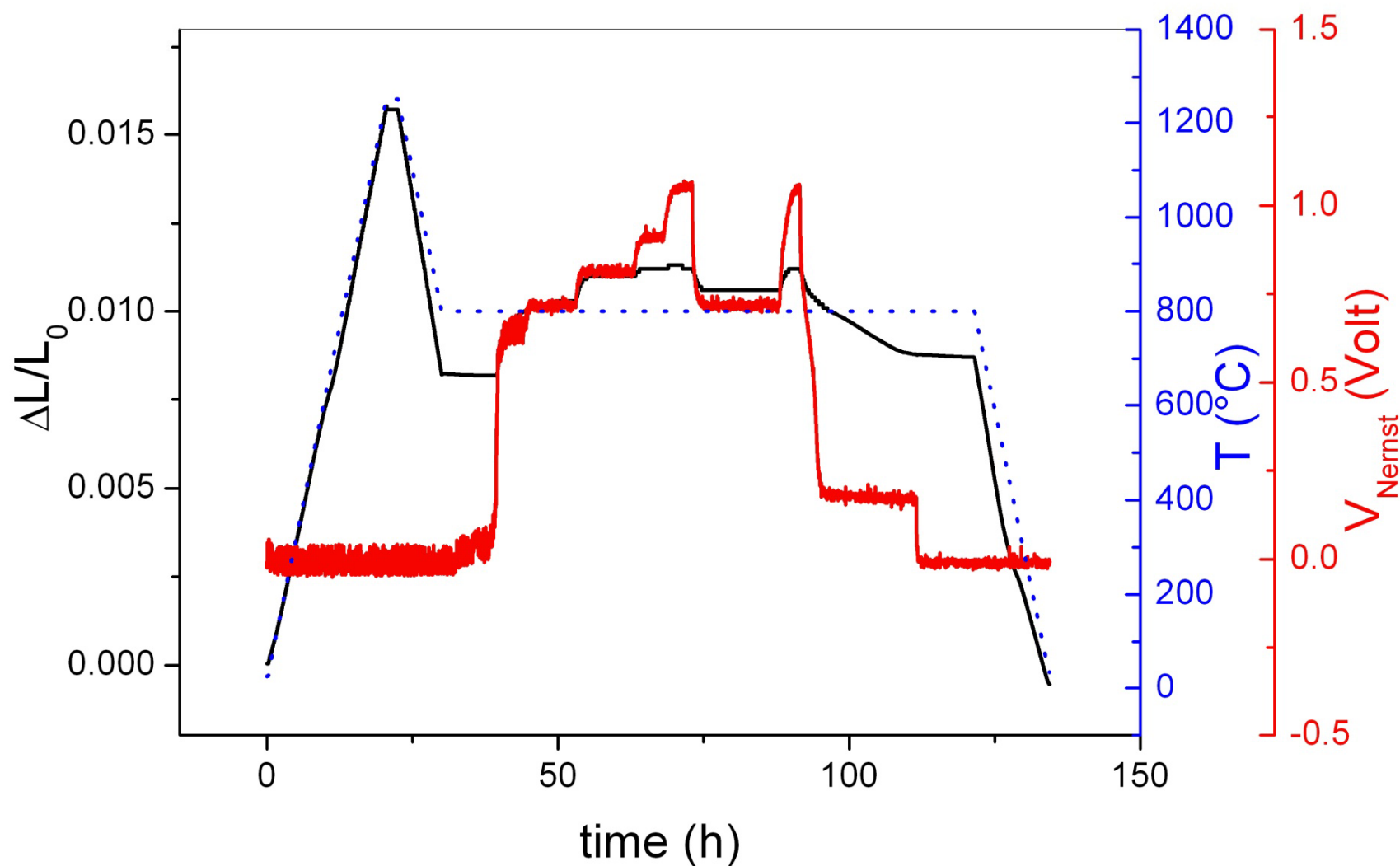




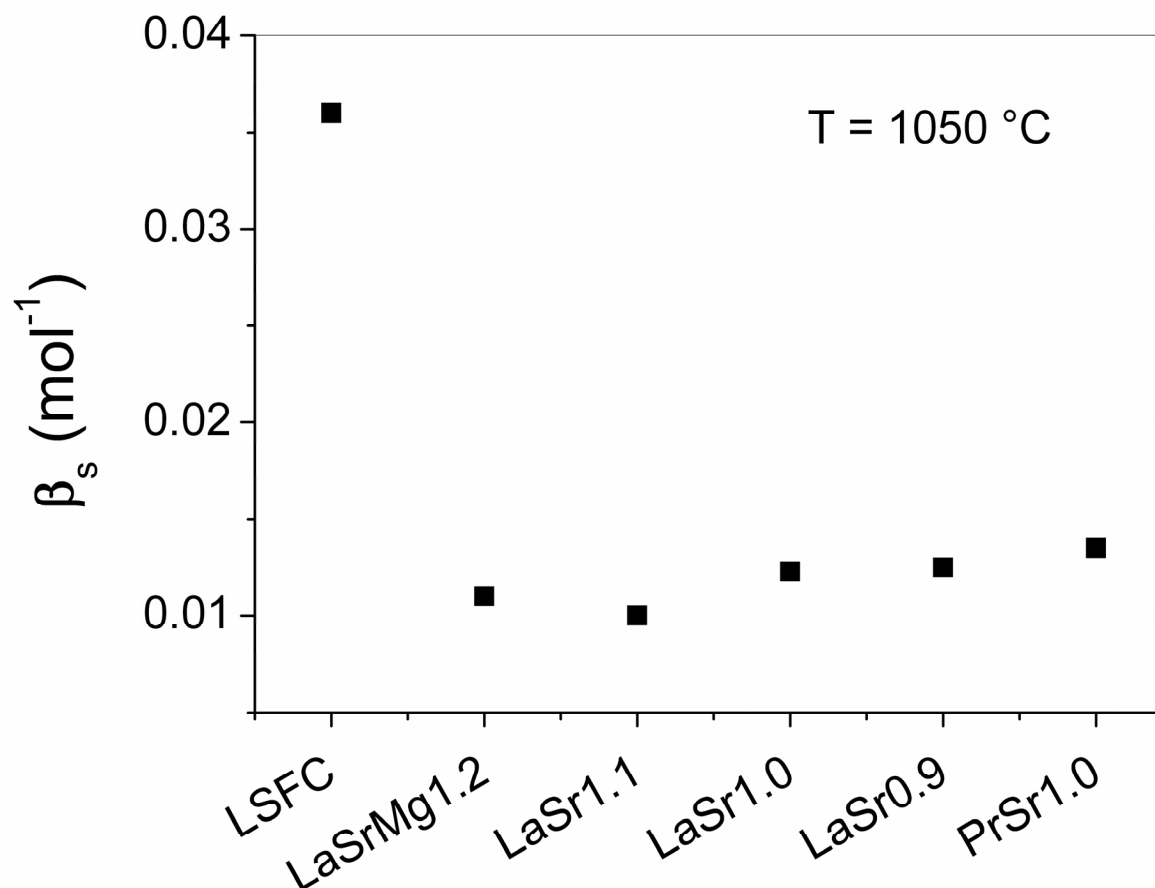
Temperature dependence of the oxygen nonstoichiometry of Ruddlesden-Popper samples in $\text{H}_2/\text{H}_2\text{O}=50$ relative to their oxygen nonstoichiometry in N_2 , estimated by thermo-gravimetry. The P_{O_2} profile is also shown as a function of temperature.

Composition	Abbreviated Name
$\text{La}_{1.08}\text{Sr}_{0.88}\text{Fe}_{0.8}\text{Co}_{0.2}\text{O}_{4-\delta}$	LaSr1.1
$\text{La}_{0.98}\text{Sr}_{0.98}\text{Fe}_{0.8}\text{Co}_{0.2}\text{O}_{4-\delta}$	LaSr1.0
$\text{La}_{0.88}\text{Sr}_{1.08}\text{Fe}_{0.8}\text{Co}_{0.2}\text{O}_{4-\delta}$	LaSr0.9
$\text{Pr}_{0.98}\text{Sr}_{0.98}\text{Fe}_{0.8}\text{Co}_{0.2}\text{O}_{4-\delta}$	PrSr1.0
$\text{Pr}_{0.78}\text{Sr}_{1.18}\text{Fe}_{0.8}\text{Co}_{0.2}\text{O}_{4-\delta}$	PrSr0.8
$\text{La}_{1.18}\text{Sr}_{0.78}\text{Fe}_{0.64}\text{Co}_{0.16}\text{Mg}_{0.2}\text{O}_{4-\delta}$	LaSrMg1.2

Dilatometry in a DIL 402CD

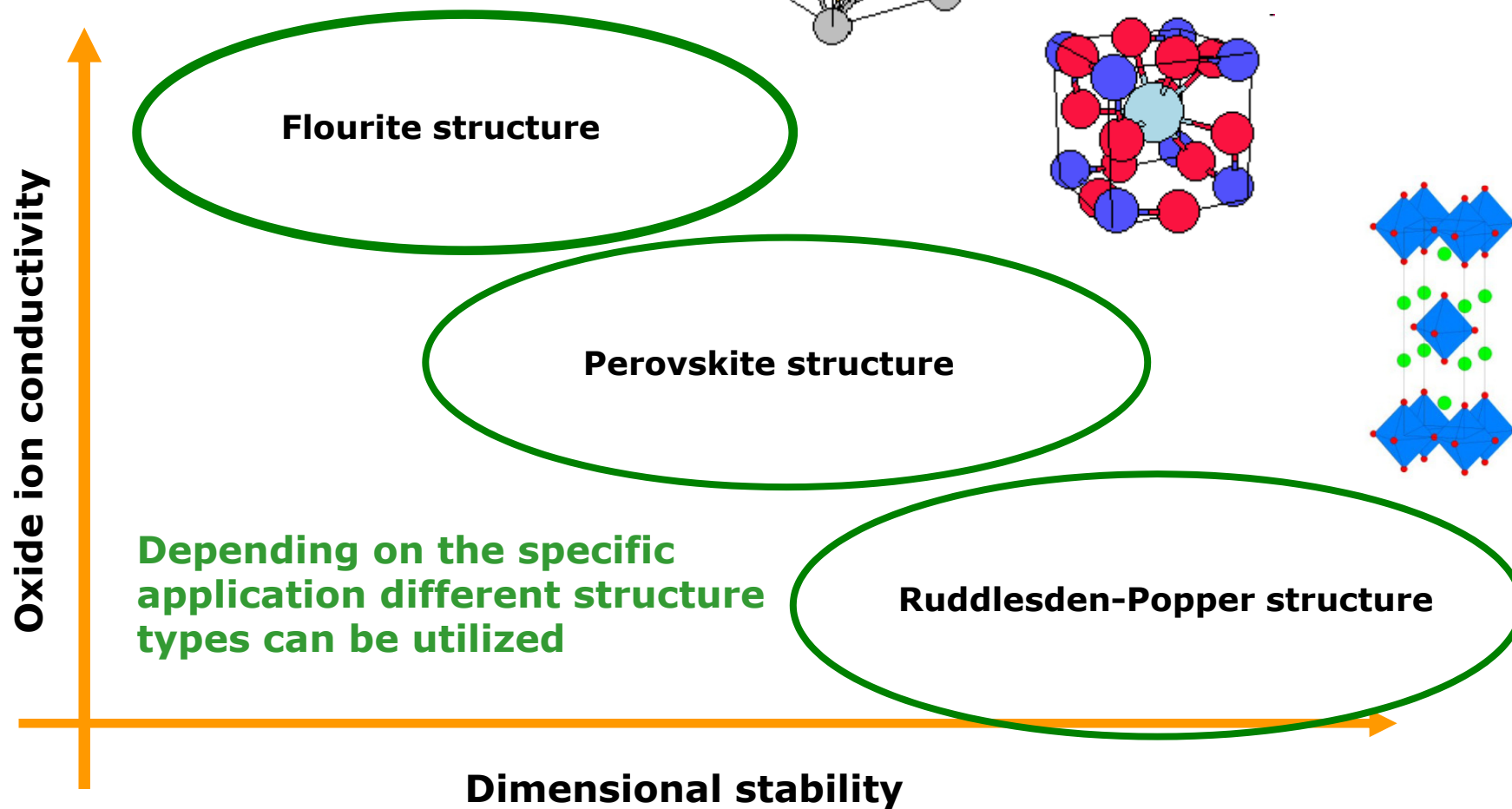


Length change of $\text{La}_{0.98}\text{Sr}_{0.98}\text{Fe}_{0.8}\text{Co}_{0.2}\text{O}_{4-\delta}$ as a function of T , $P_{\text{O}_2}(V_{\text{Nernst}})$

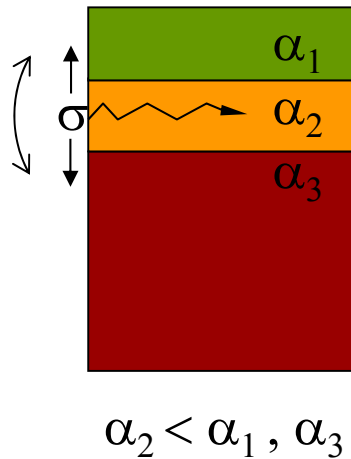
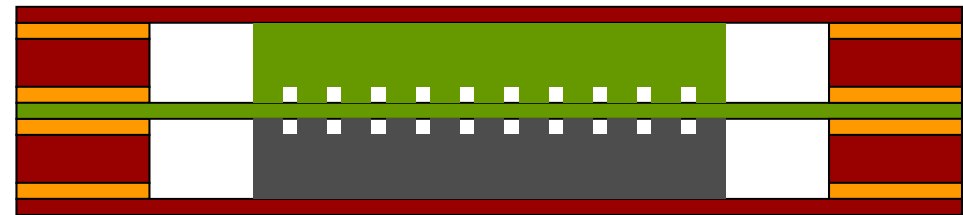
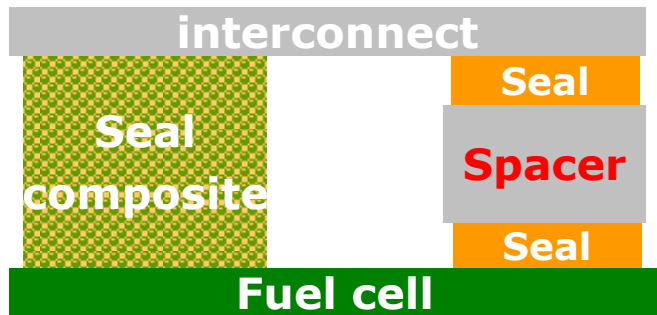


Chemical expansion coefficient of the various single phase Ruddlesden-Popper compositions measured at 1050 °C using air/CO₂/H₂ mixtures. The corresponding value of the perovskite (La_{0.6}Sr_{0.4})_{0.99}Fe_{0.8}Co_{0.2}O_{3- δ} (LSFC) measured at 800 °C using air/CO₂ mixtures is also shown for comparison.

Materials

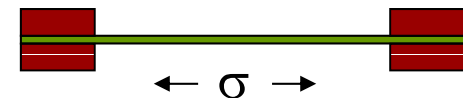


Seal design and thermally induced stresses



Seal Edge Fracture

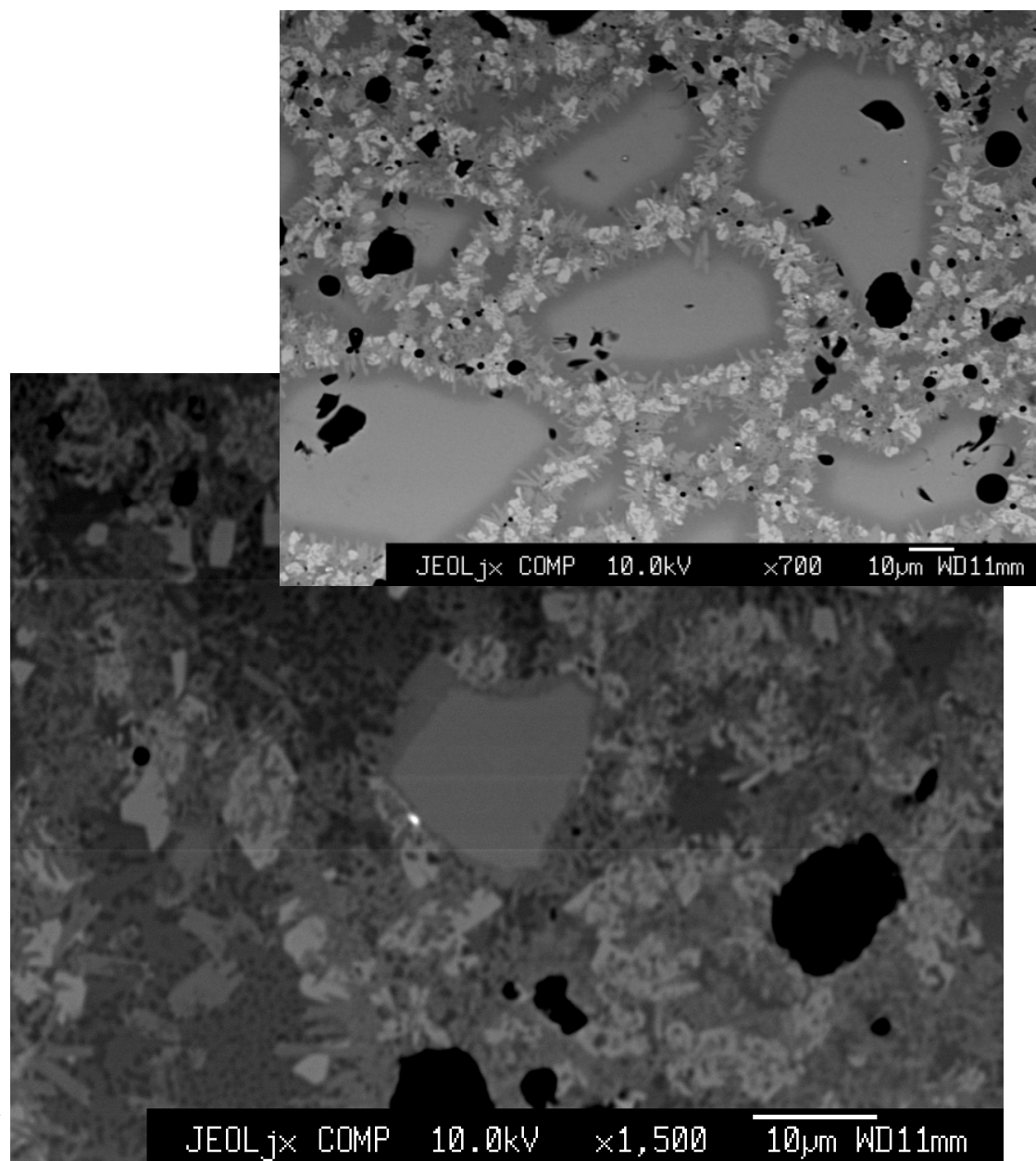
Assembly Stress



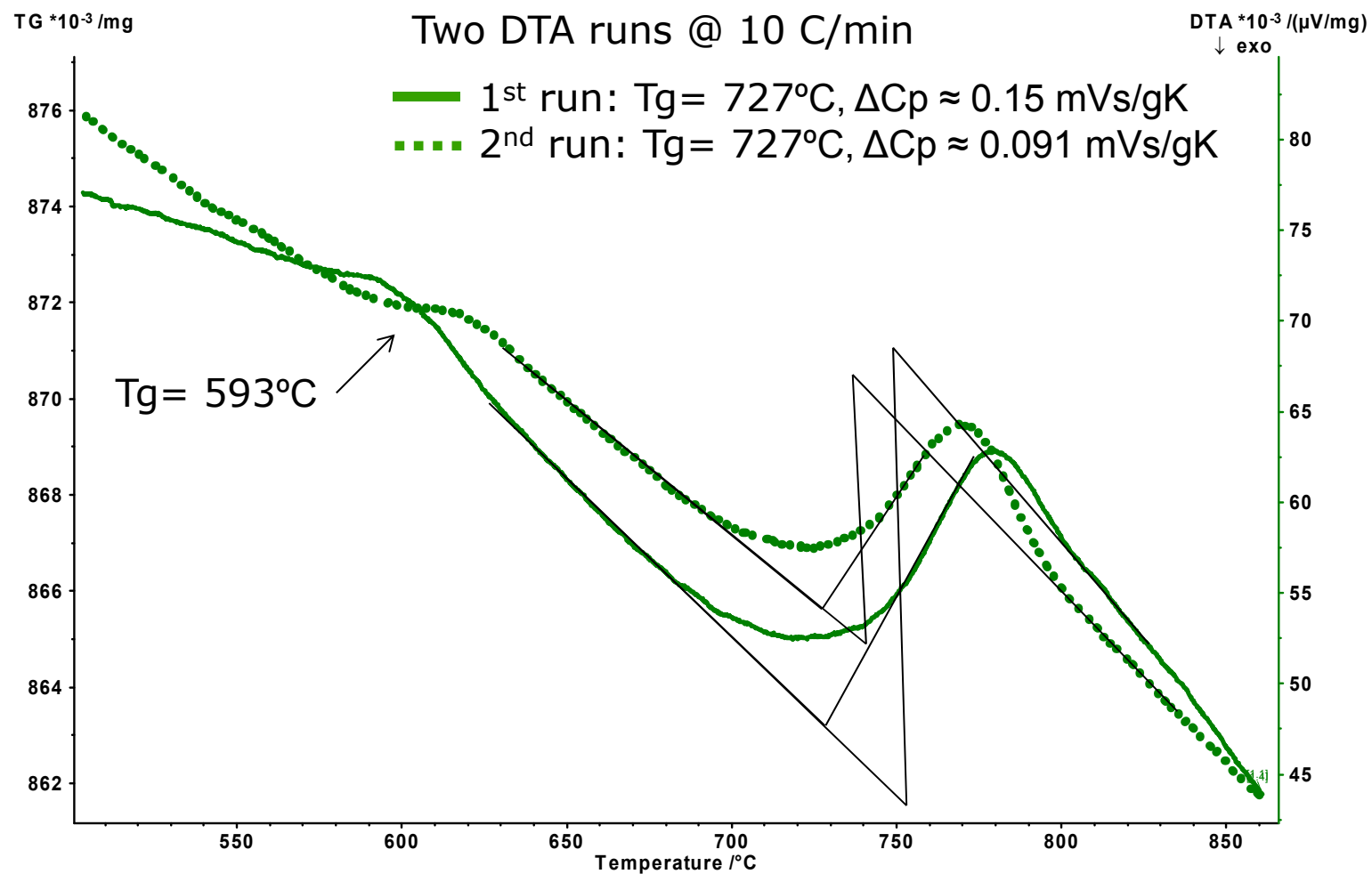
Soda lime magnesia aluminoborosilicate glass

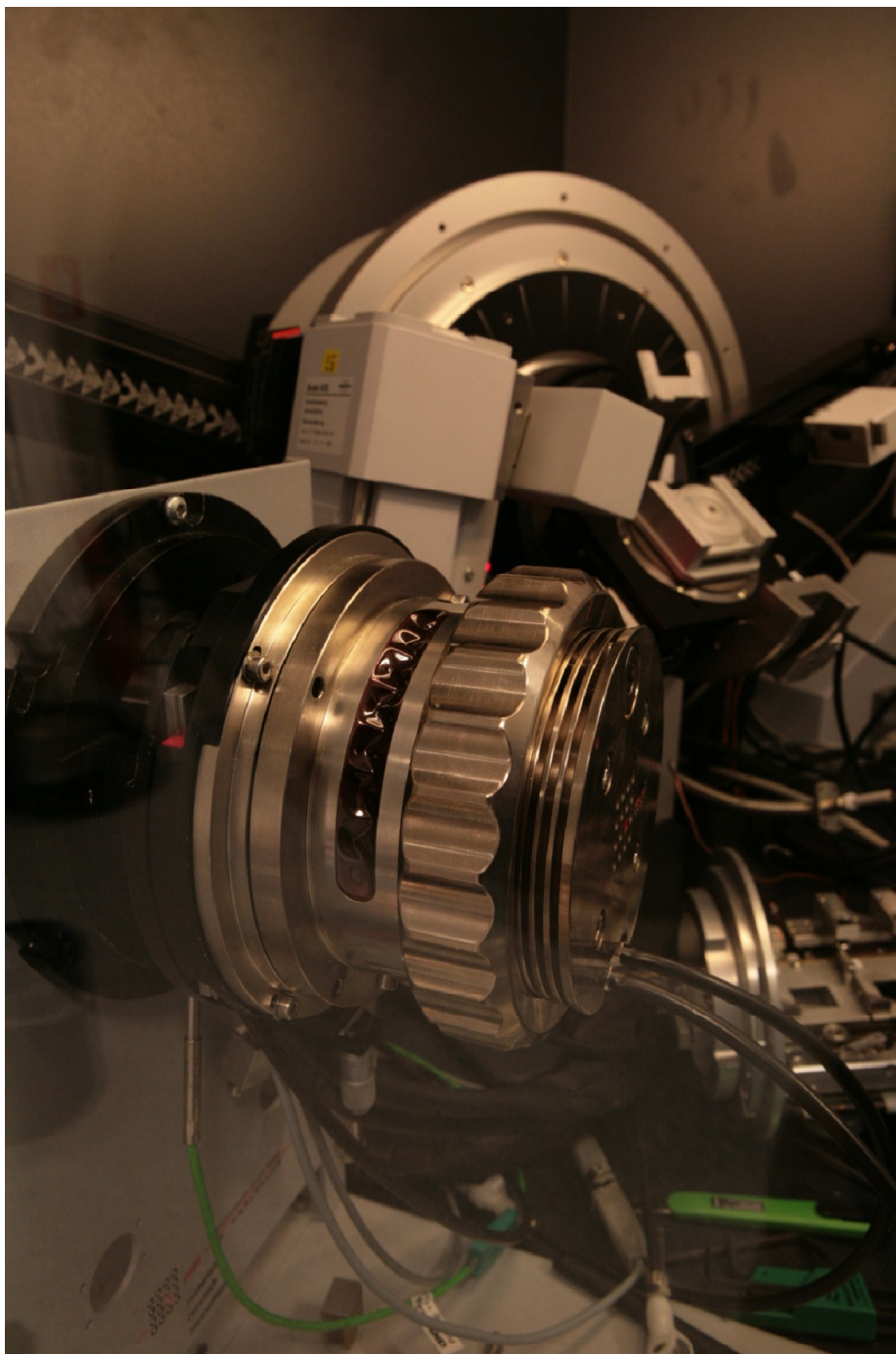
Addition of a filler material with high CTE increases CTE of the crystallized glass. Filler and glass may behave independently

- **Using amorphous SiO_2 as filler increases the part of the glass that crystallizes to cristoballite**
- **The CTE can be increased from $8\text{--}10 \times 10^{-6} \text{ K}^{-1}$ to about $11\text{--}12 \times 10^{-6} \text{ K}^{-1}$**
- **Using crystalline SiO_2 as filler facilitates crystallisation of an increased amount of Quartz, which also increases CTE to desired levels**



Glass transition, Glass P





Bruker D8
with hot stage from
MRI, Karlsruhe
(<1400°C)

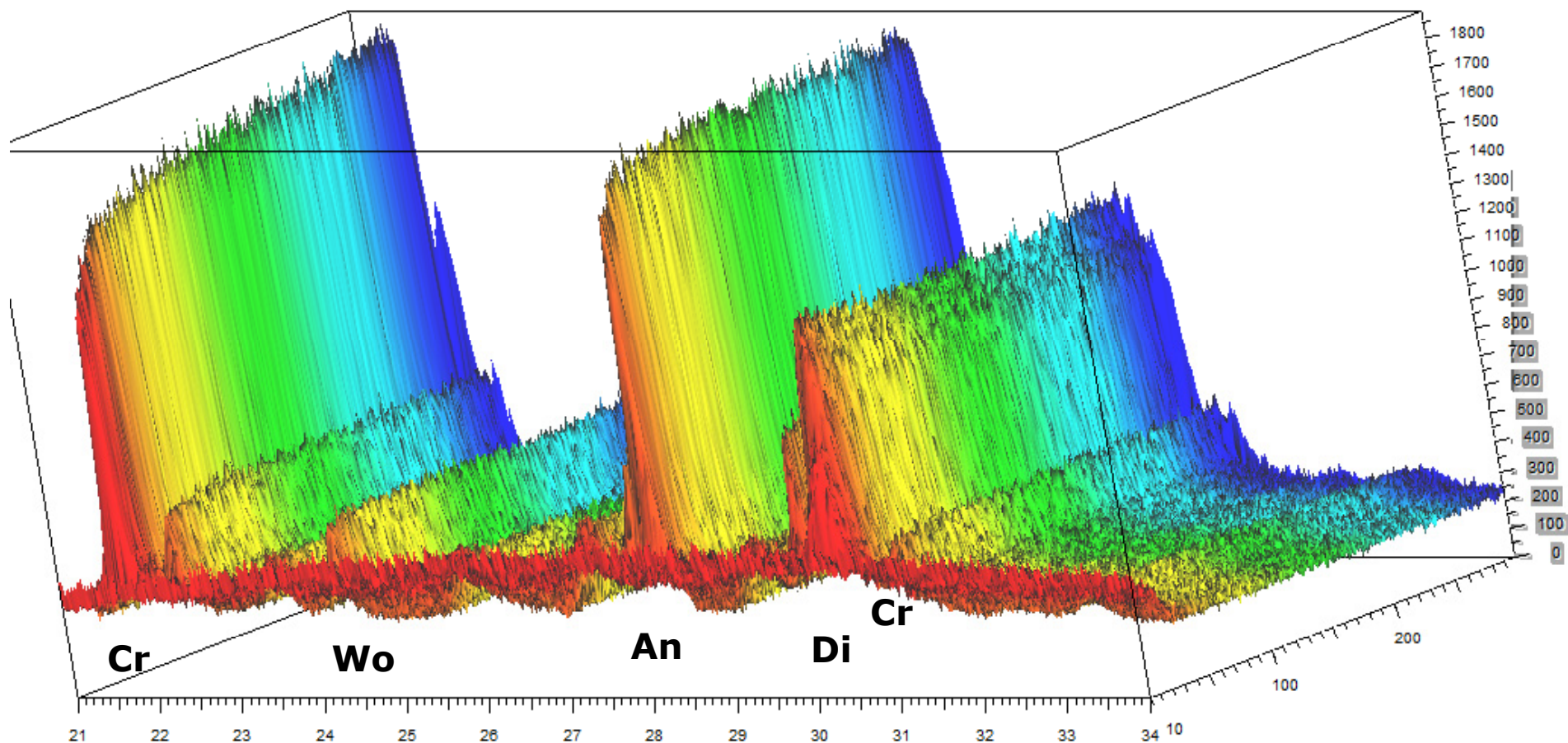
Glass P, XRD @ 900°C for 60h

Cristobalite: SiO_2

Wollastonite: $\text{Ca}_3\text{Si}_3\text{O}_9$

Diopside: $\text{CaMgSi}_2\text{O}_6$

Anorthite: $\text{CaAl}_2\text{Si}_2\text{O}_8$



Glass Sz, XRD @ 900°C for 60h

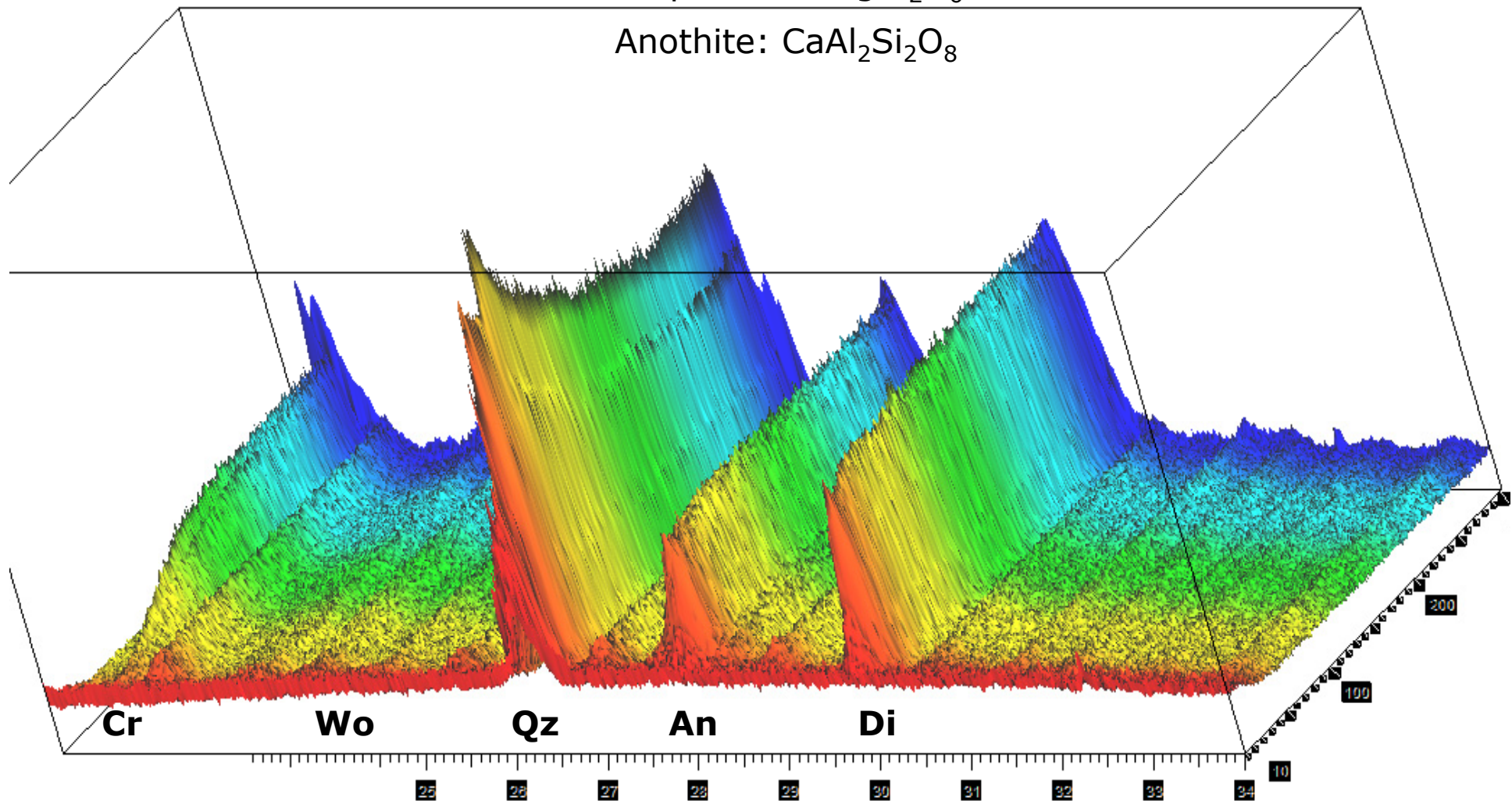
Quartz: SiO_2

Wollastonite: $\text{Ca}_3\text{Si}_3\text{O}_9$

Cristobalite: SiO_2

Diopside: $\text{CaMgSi}_2\text{O}_6$

Anothite: $\text{CaAl}_2\text{Si}_2\text{O}_8$



Conclusions



Thermal analysis encompasses a number of techniques, useful in materials research when combined.

Magneto-DSC and CATH-SPM were build to meet targeted purposes and extending the range of commercial instruments.

Optical dilatometry, or contact-free dilatometry supplements conventional TA-instruments, when looking into behaviour of multilayer ceramics.

Symmetrical instruments, DIL402CD and TG439, are efficient tools for running longer and complicated heating and gas composition profiles as when studying gas-solid reactions.

Kinetic analysis is a useful tool for acquiring rough numbers to optimise processing profiles and is at best when combined with common sense and experience.

More detailed information on crystallisation of glasses can be acquired through high temperature XRD than through DSC/DTA

Thank you for your attention

My gratitude goes to colleagues at the department, in particular to Carsten Gynter Sørensen and Pernille Hedemark for helping with experiments and to Christos Chatzichristodoulou, Stinus Jeppesen, Christian Bahl, De Wei Ni, Karin Vels and Mouritz Svendsen for sharing experimental results.